

**Transmission System Impact Study Results
for Group 3 of Distributed Energy
Resource (DER) Additions in Western
Massachusetts**

June 2022

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1 EXECUTIVE SUMMARY

This document provides the transmission system impact study results for Group 3 of National Grid's Western MA DER interconnection cluster study. Group 3 consists of the third stage of proposed Distributed Energy Resources (DER) additions applying for interconnection into the National Grid distribution system in Western MA. Groups 1 and 2 (previously approved) consisted of 314 MW of DER in Western Massachusetts, after accounting for all project attrition. None of Group 1 and 2 DER can charge from the transmission grid. Group 3 consists of an additional 252 MW of DER in Western MA, of which 121 MW can charge from the transmission system.

The following table shows the Group 3 DER broken down by Generation type.

Table 1 - Group 3 DER by Generation Type

| Generation Type | Group 3 Total PV + BESS Discharging Limit¹ (kW) | Group 3 Total BESS Charging Limit² (kW) |
|------------------------|---|---|
| PV Only | 9,998 | N/A |
| BESS Only | 164,750 | 113,550 |
| PV+DC BESS* | 51,681 | 6,150 |
| PV+AC BESS** | 25,448 | 1,000 |
| Grand Total | 251,877 | 120,700 |

*With DC coupled PV+BESS, the PV and BESS share the same inverter

** With AC coupled PV+BESS, the PV and BESS are each equipped with dedicated inverters

Results of the steady state analysis indicate the the following Transmission upgrades need to be made to accommodate the integration of the Group 3 DER,

- **A1/B2 line rebuild/reconductor:** The A1/B2 69 kV transmission lines were found to overload following the addition of Group 3 DER. These overloads will be eliminated following the rebuild of both lines that is already planned due to asset condition issues. The lines will be rebuilt using 795 ACSS conductor. The refurbishment is scheduled to be completed in 2027.
- **Royalston Breaker Additions:** Voltage problems were identified at several substations along the A1/B2 lines following the addition of Group 3 DER. 69 kV breaker additions at Royalston substation, already planned as part of the A1/B2 rebuild project, will resolve these high voltage problems.

¹ Discharging limit imposed by distribution system constraints

² Charging limit imposed by distribution system constraints

- **Vernon 69 kV substation rebuild:** A-1 and B-2 69 kV terminal equipment at Vernon substation were found to overload following the addition of Group 3 DER. There is presently an asset condition project planned to rebuild Vernon station (to be renamed “Huntington” substation) which will eliminate the overloads. The rebuild is scheduled to be completed in 2026.
- **E5/F6 line rebuild/reconductor:** The E-5/F-6 69 kV transmission lines were found to overload following the addition of Group 3 DER if [REDACTED] Solar (QP1031) is built. These overloads will be eliminated following the rebuild of both E5/F6 lines, already scheduled to address asset condition issues on the lines. The lines will be rebuilt using 795 ACSS conductor. The rebuild project is scheduled to be completed in 2030. Note that if QP1031 is withdrawn, Group 3 DER alone does not cause the E5/F6 lines to become overloaded.

Transient stability, short circuit, and PSCAD analyses were also conducted during this study, and no issues were identified.

2 INTRODUCTION

This document provides the system impact study results for the interconnection of 252 MW of Distributed Energy Resources (DER), greater than 1 MW, into the Western Massachusetts distribution system, owned by National Grid, over the years 2022 to 2025. Below are some additional characteristics of the Group 3 DER:

- None of the additional DER will be directly connected to the transmission system.
- All the DER will be mixed with distribution load.
- None of the additional DER will control voltage.
- All DER was set to a power factor of unity in the study.
- All the DER will respond to frequency deviations.

2.1 Study Objective

The objective of this study is to identify the transmission upgrades, if any, required to integrate the proposed DER without resulting in any significant adverse impact on the reliability, stability, and operating characteristic of the New England bulk power transmission system and National Grid transmission system.

2.2 Project Description

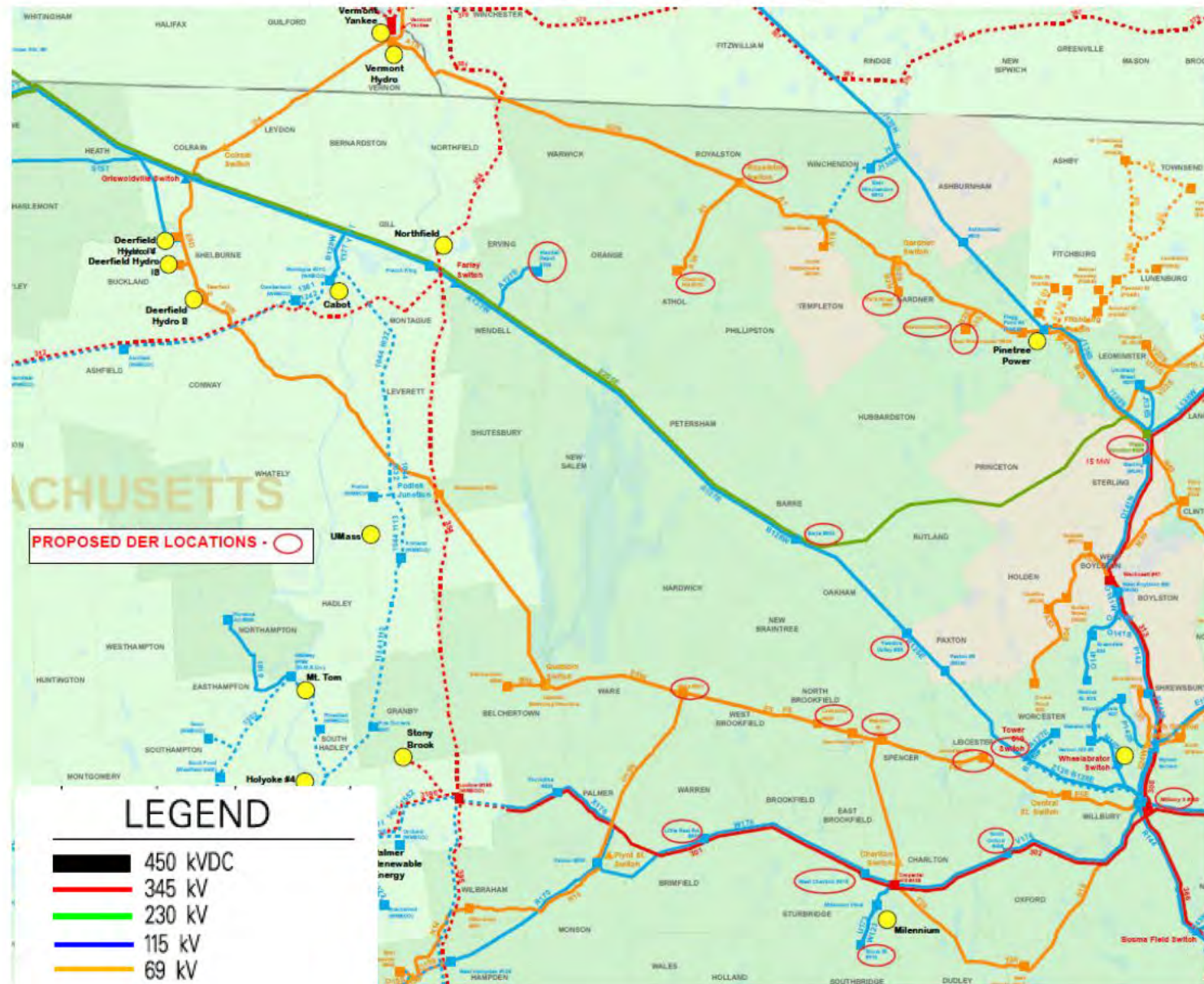
252 MW of DER (>1 MW) have applied to interconnect to the National Grid distribution system in Western MA by 2025.

2.3 Study Area

The transmission system geographic map and one-line diagram of the study area are shown in the following figures, with the DER project locations identified.

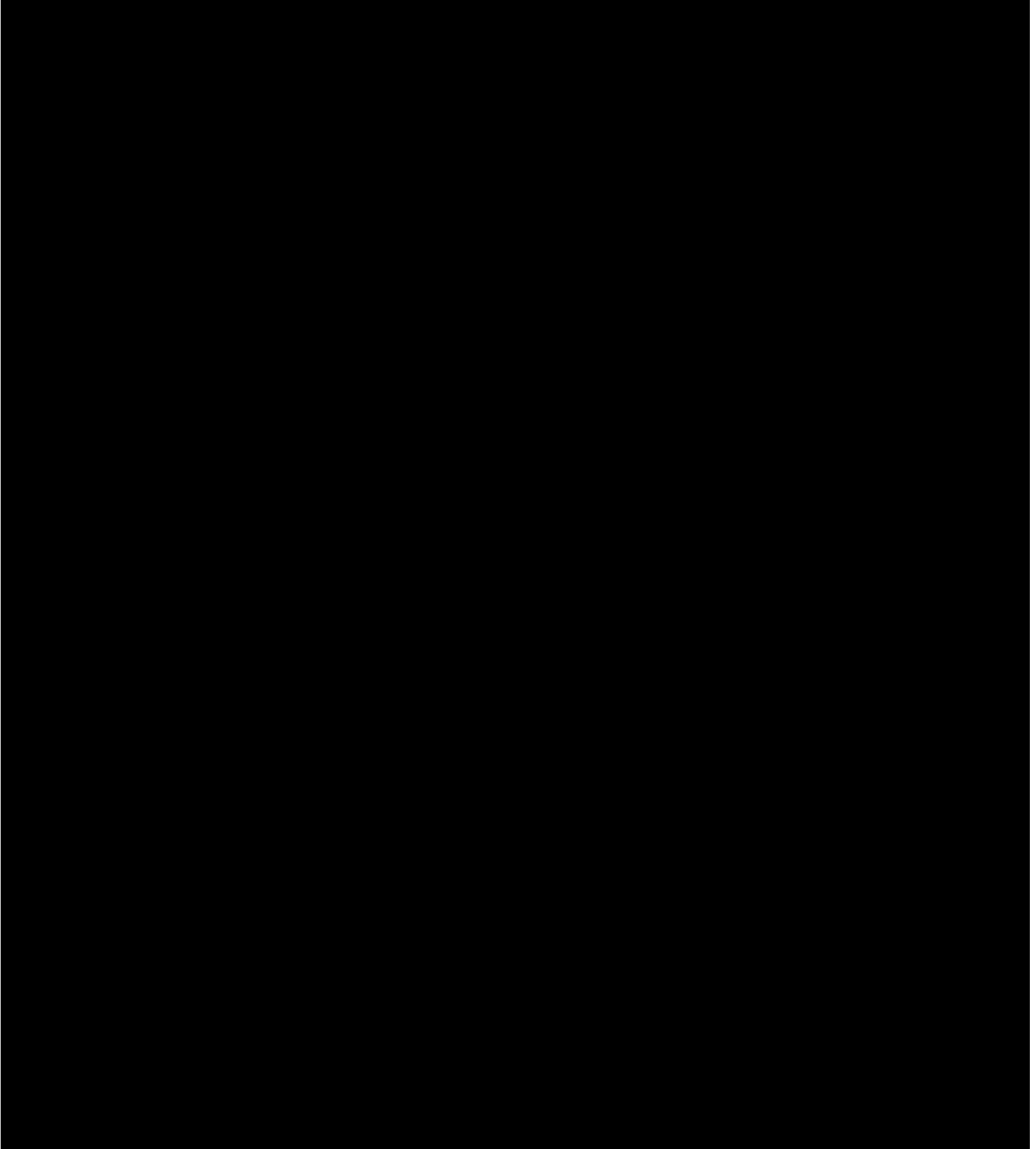
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Figure 1 - Proposed DER Locations - Geographic Map



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Figure 2 - Proposed DER locations for Group 3 - One Line Diagram



3 STUDY APPROACH

DER additions 1 MW and below, did not need to be added to the base cases for this study. The base cases utilized for this study already modeled DER 1 MW and below, via negative loads (with “PD” identifiers) that model the forecasted PV, 1 MW and below, out to year 2025. This DER, 1 MW and below, is distributed proportionally across the load busses in Western Massachusetts. Therefore, only DER additions that exceed 1 MW, were added to the cases utilized for this study. All 252 MW associated with Group 3 is greater than 1 MW.

3.1 Group 3 Totals by Substation

The Group 3 total amounts to 252 MW of new DER, and constitutes the third increment of National Grid DER studied in Western MA. The DER totals for Group 3 are shown in the following table for each substation.

Table 2 - Group 3 Total DER by Substation

| Substation | Generation Type | Group 3 Total PV + BESS Discharging Limit ³ (kW) | Group 3 Total BESS Charging Limit ⁴ (kW) |
|------------------------------|-----------------|---|---|
| BARRE SUBSTATION | Battery only | 8,000 | 8,000 |
| | DC coupled | 4,400 | 3,150 |
| Crystal Lake SUBSTATION | Battery only | 8,000 | 5,200 |
| E. WESTMINSTER SUBSTATION | DC coupled | 4,990 | 3,000 |
| E. WINCHENDON SUBSTATION | Battery only | 14,900 | 8,800 |
| | PV Only | 4,999 | N/A |
| LASHAWAY SUBSTATION | Battery only | 15,000 | 12,000 |
| LITTLE REST RD SUBSTATION | AC Coupled | 3,000 | 0 |
| | DC coupled | 2,800 | 0 |
| MEADOW STREET 552 SUBSTATION | DC coupled | 8,800 | 0 |
| | PV Only | 4,999 | N/A |
| MILLBURY SUBSTATION | AC Coupled | 2,750 | 0 |
| | Battery only | 10,000 | 3,500 |
| N. OXFORD SUBSTATION | Battery only | 13,600 | 11,200 |
| | DC coupled | 4,400 | 0 |
| PRATTS JUNC. SUBSTATION | Battery only | 11,000 | 7,000 |
| ROYALSTON SUBSTATION | AC Coupled | 7,500 | 0 |
| SNOW ST. SUBSTATION | AC Coupled | 4,998 | 1,000 |
| | Battery only | 18,250 | 14,750 |
| STAFFORD ST SUBSTATION-New | Battery only | 10,000 | 10,000 |
| | DC coupled | 12,500 | 0 |
| TREASURE VALLEY SUBSTATION | Battery only | 10,000 | 5,000 |
| W. CHARLTON SUBSTATION | Battery only | 20,000 | 8,500 |
| WARE SUBSTATION | DC coupled | 11,000 | 0 |
| WENDELL DEPOT SUBSTATION | AC Coupled | 7,200 | 0 |
| | Battery only | 18,000 | 15,200 |
| | DC coupled | 2,791 | 0 |
| LAUREL CIRCLE SUBSTATION | Battery only | 8,000 | 4,400 |
| Grand Total | | 251,877 | 120,700 |

³ Discharging Limits imposed by distribution system constraints

⁴ Charging Limits imposed by distribution system constraints

The total DER studied for the Group 3 Western MA Cluster study amounts to 252 MW. This DER is incremental to the DER in Groups 1 and 2 of the Western Massachusetts Cluster, which amounted to 314 MW, after accounting for all project attrition within the clusters. No DER in Groups 1 and 2 can charge from the transmission system. The totals for Groups 1 and 2 are shown in the following table for each substation.

Table 3 – Group 1 + 2 DER Totals by Substation, Post Attrition

| Substation for Groups 1 + 2 | Total MW |
|------------------------------------|-----------------|
| ADAMS SUBSTATION | 11 |
| ASHBURNHAM SUBSTATION | 5 |
| BARRE SUBSTATION | 12.4 |
| BEAR SWAMP UPPER YARD SUBSTATION | 2.5 |
| BELCHERTOWN SUBSTATION | 8 |
| CHESTNUT HILL 702 SUBSTATION | 3.3 |
| Crystal Lake SUBSTATION | 24.7 |
| E. WEBSTER SUBSTATION | 5 |
| E. WESTMINSTER SUBSTATION | 8 |
| E. WINCHENDON SUBSTATION | 3.9 |
| EAST LONGMEADOW SUBSTATION | 9 |
| FIVE CORNERS SUBSTATION | 3 |
| LASHAWAY SUBSTATION | 13.7 |
| LEICESTER SUBSTATION | 2.6 |
| LITCHFIELD ST SUBSTATION | 10 |
| LITTLE REST RD SUBSTATION | 6 |
| MEADOW STREET 552 SUBSTATION | 13.4 |
| MILLBURY SUBSTATION | 14.4 |
| N. OXFORD SUBSTATION | 8.7 |
| PALMER 503 SUBSTATION | 18 |
| PONDVILLE SUBSTATION | 4.9 |
| SHUTESBURY | 20 |
| SNOW ST. SUBSTATION | 24.7 |
| THORNDIKE SUBSTATION | 12.5 |
| TREASURE VALLEY SUBSTATION | 2.2 |
| W. CHARLTON SUBSTATION | 17 |
| WARE SUBSTATION | 13.3 |
| WENDELL DEPOT SUBSTATION | 15 |
| West Hampden 139 SUBSTATION | 13.2 |
| WESTMINSTER SUBSTATION | 4.9 |
| WILBRAHAM SUBSTATION | 4 |
| Total | 314 |

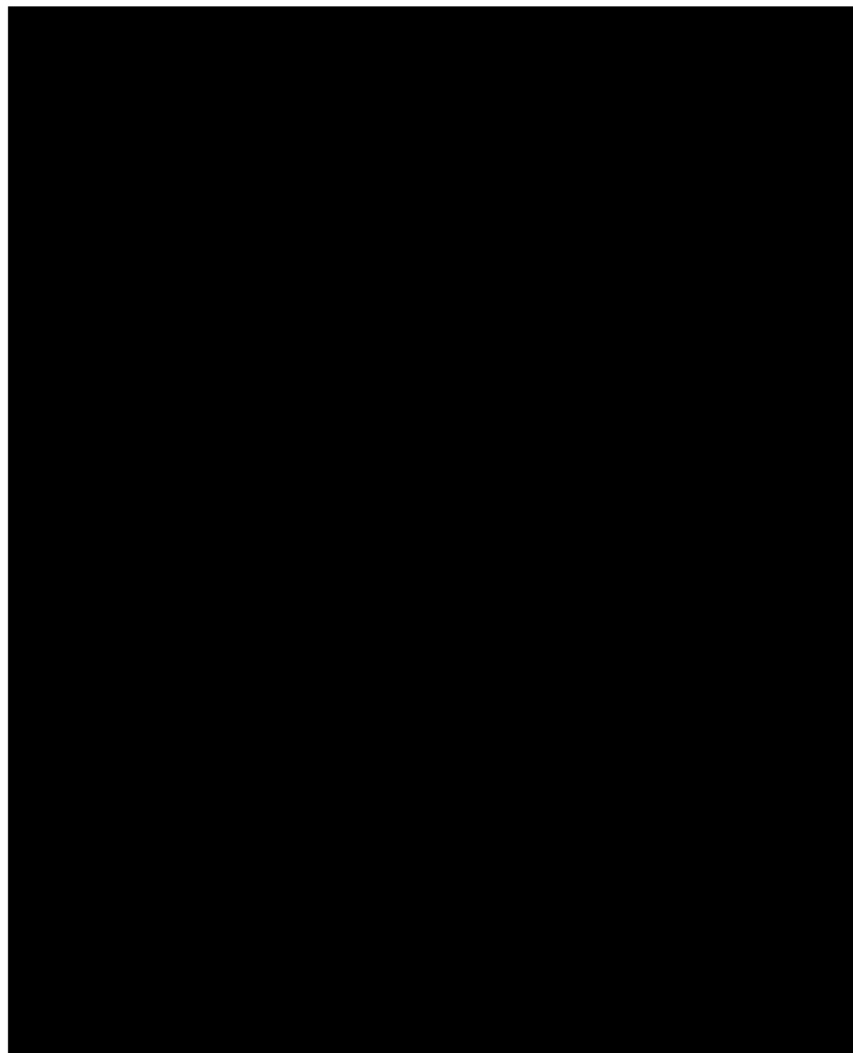
3.2 Distribution Substation Upgrades

Several distribution substation upgrades will need to be built in order to accommodate the interconnection of the Group 3 DER into the Western MA Distribution system:

Wendel Depot Substation

A second 115/13.8 kV transformer [REDACTED] will be installed, as well as the replacement of the existing 115/13.8 kV transformer [REDACTED]

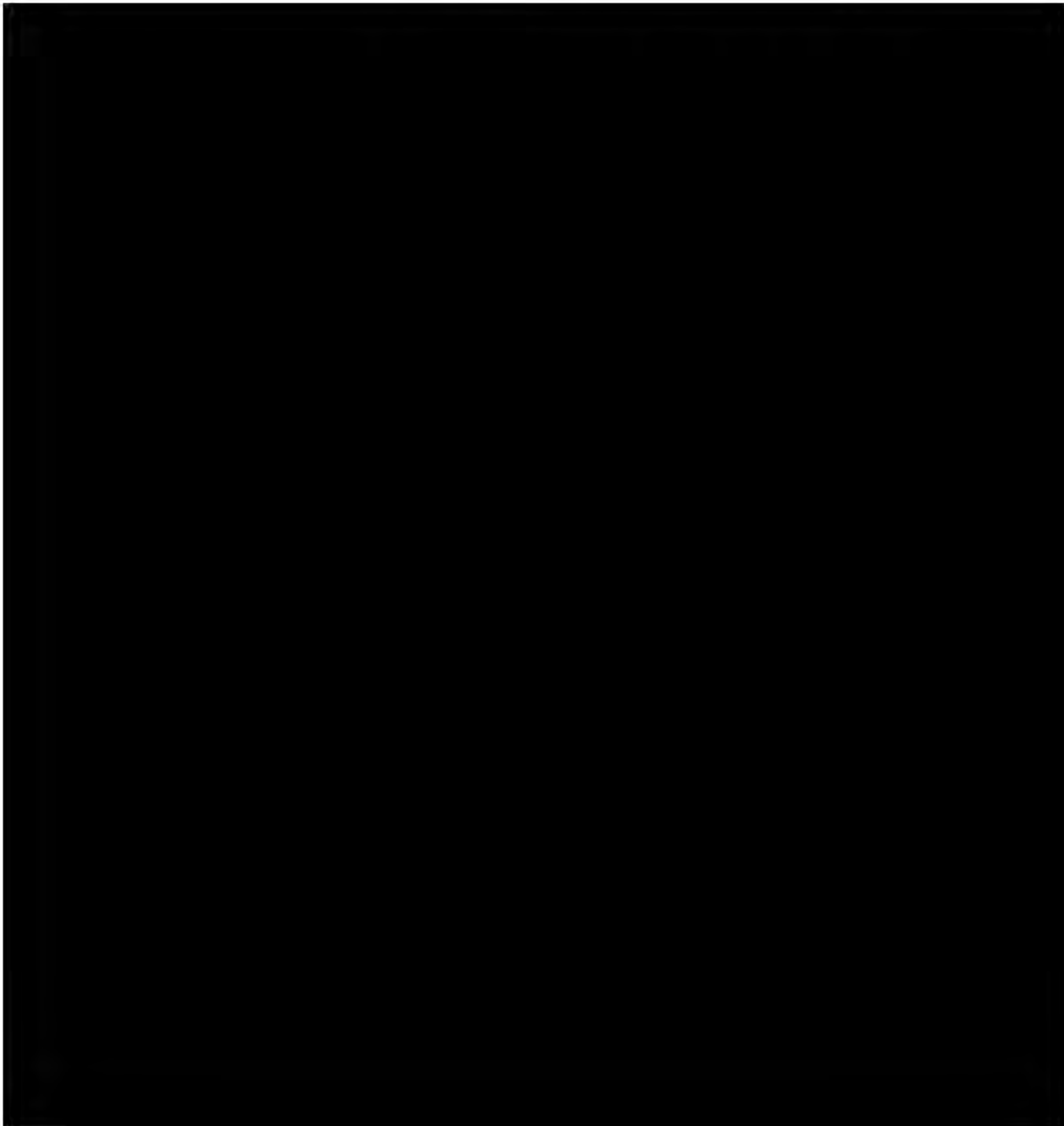
Figure 3 – Wendel Depot Substation Upgrades



E Winchendon Substation

Replace existing 115/13.8 kV transformer with a [REDACTED]

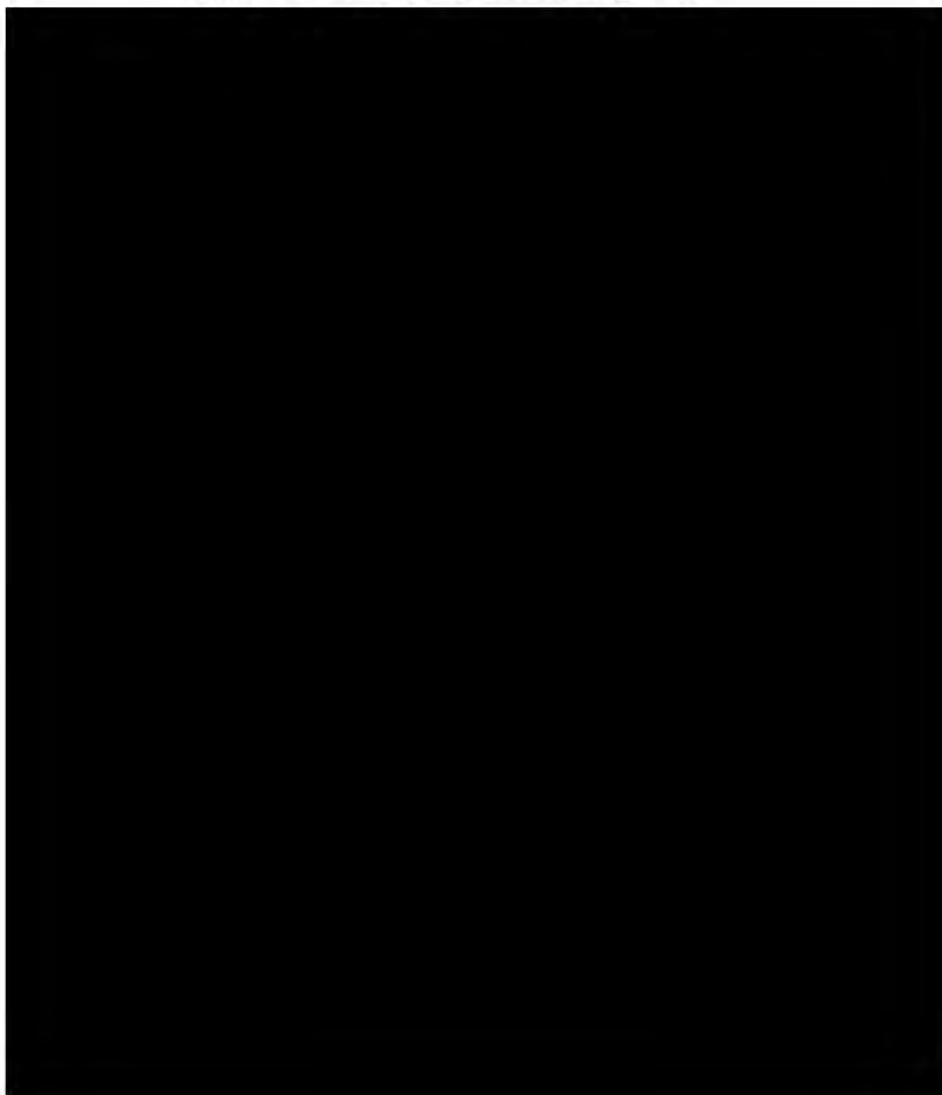
Figure 4 – E Winchendon Substation Upgrades



Barre Substation

Replace both existing 115/13.8 kV transformers with [REDACTED]

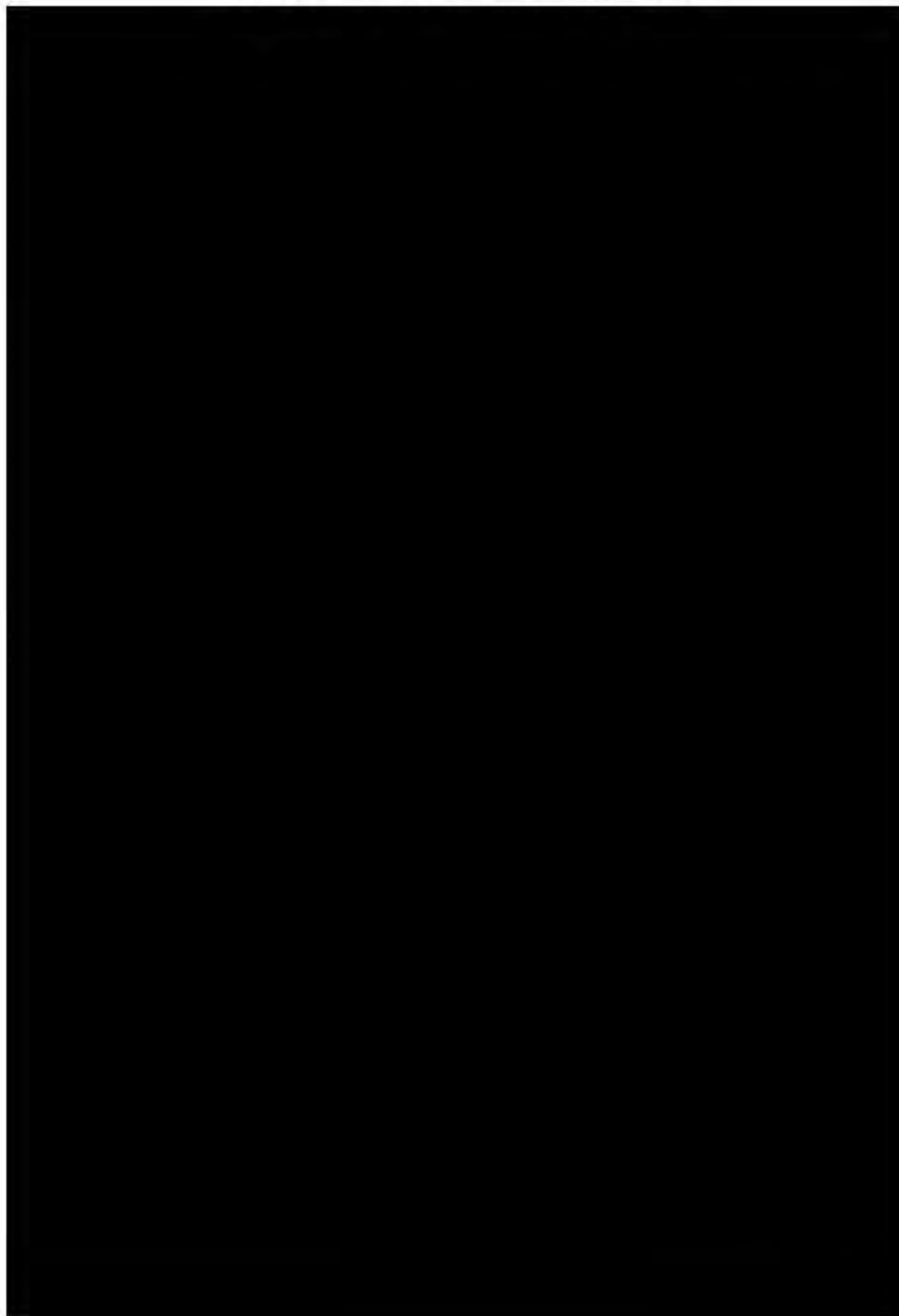
Figure 5 – Barre Substation Upgrades



Ware Substation

Replace existing 69/23 kV transformer with 69/13.8 kV [REDACTED].

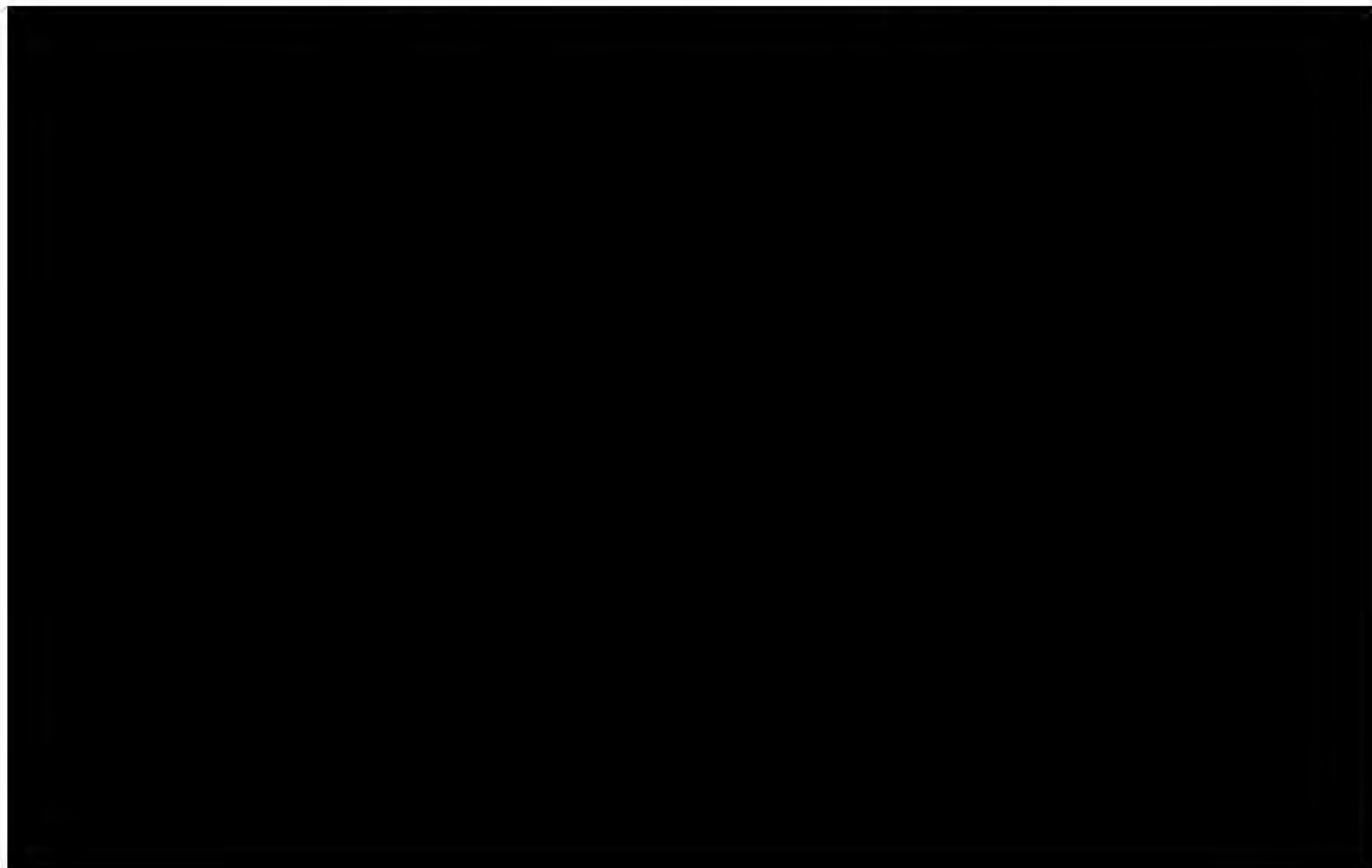
Figure 6 – Ware Substation Upgrades



Meadow St Substation

Install a second 69/13.2 kV transformer () and install 69 kV breaker.

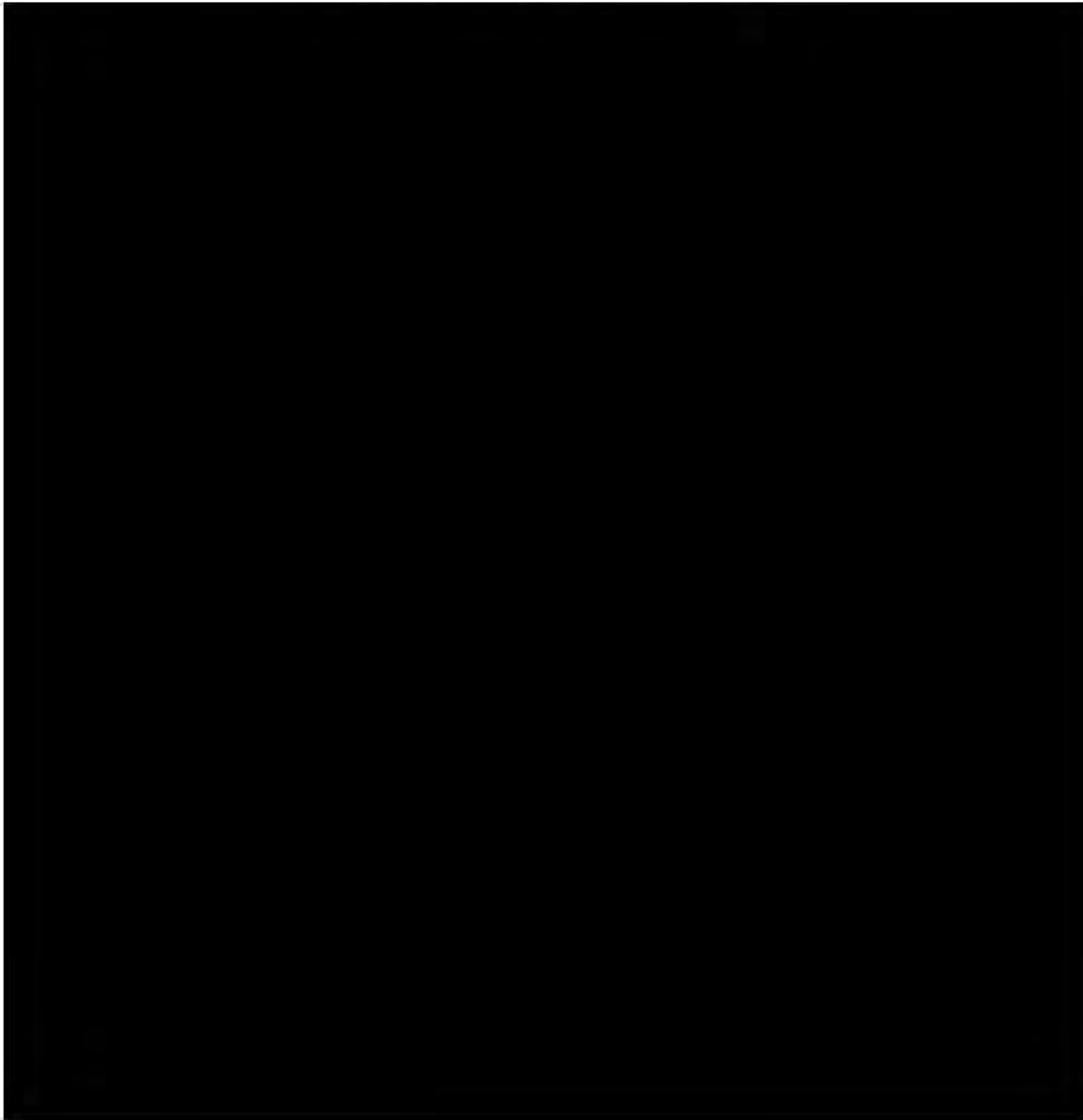
Figure 7 – Meadow St Substation Upgrades



Lashaway Substation

Replace the existing 69/13.2 kV transformer with a [REDACTED] unit, and replace the existing 69/23kV transformer with a 69/13.2 kV transformer ([REDACTED])

Figure 8 – Lashaway Substation Upgrades



Leicester 69/13.8kV substation - Retire

3.3 Study Assumptions

- DER was dispatched as follows in both the steady state base cases, as well as the stability base cases:
 - All the Group 1, 2, and 3 DER in this study, greater than 1 MW, were added to the cases, and dispatched at 100% nameplate, at all load levels. This DER is modeled with negative load⁵ at each distribution bus for the substations listed in Table 3. No distribution feeder impedance is assumed.
 - For the purposes of describing the treatment of existing and forecasted PV in the study, PV is placed into three categories:
 - All existing Category 1 PV (existing or PPA approved PV facilities greater than or equal to 5 MW) in the 2025 base case representation provided by ISO-NE, was dispatched at 100 % output for all load levels.
 - All existing Category 2 PV (existing PV facilities greater than 1 MW and less than 5 MW) provided by ISO-NE with the 2025 base cases, is dispatched at 100 % output at the peak load level only. No Category 2 PV was modeled in the light load and intermediate load cases.
 - All existing Category 3 PV (Existing facilities less than or equal to 1 MW and all future forecasted solar PV for which locational information is not available) provided by ISO-NE with the 2025 base cases, is dispatched at 100 % output at the peak load level only. Note that the “future” solar PV greater than 1 MW and less than 5 MW is carved out of the Category 3 PV to avoid double counting of the new DER for which this study is being conducted. No Category 3 PV was modeled in the light load and intermediate load cases.
- None of the DER additions were modeled in voltage control mode, since all of the new DER will be mixed with distribution load (i.e., no DER will be installed on dedicated feeders)
- All of the Group 3 DER will be operated in frequency response mode (per the new Source Requirements Document (SRD) developed for Group 3). None of the Group 1 and Group 2 DER will be operated in frequency response mode (per the previous SRD in place during the Group 1 and Group 2 studies). Therefore, the DER additions for each group were modeled accordingly in the stability study.
- No transmission ring busses are required for any DER additions that are mixed with distribution load, or will be mixed with distribution load in the future.
- Starting from the original base cases developed for this study, and prior to testing any contingencies, the Group 1, 2 and 3 DER was dispatched (at 100% output) against existing (and PPA approved) non-DER generation in Connecticut. This maintained the same transfer levels (pre vs post DER additions) of interfaces relevant to this study (i.e., E-W and NY-NE).

⁵ DER was modeled as generators in the load flow base cases utilized for the stability testing

- Treatment of transmission overloads above 100 kV in study:

- [REDACTED]
[REDACTED]
[REDACTED]
[REDACTED] [REDACTED]

- [REDACTED]
[REDACTED]
[REDACTED]

- [REDACTED]
[REDACTED]

- Treatment of transmission overloads below 100 kV in study:

- [REDACTED]
[REDACTED]

- [REDACTED]
[REDACTED]
[REDACTED]
[REDACTED] [REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]

⁶ This is consistent with the Minimum Interconnection Standard (MIS) outlined by FERC Order 2003.

Table 4 - Generators Available for Redispatch to Prevent 69 kV Overloads

| PSSE Bus number | Generator Name |
|-----------------|----------------|
| 109296 | Sears Wind_E |
| 109297 | Sears Wind_W |
| 109403 | Drfld East G |
| 109404 | Drfld West G |
| 109503 | Harriman G3 |
| 109504 | Harriman G2 |
| 109505 | Harriman G1 |
| 109517 | Sears Hydro |
| 109529 | Vernon Hyd A |
| 109530 | Vernon Hyd B |
| 109531 | Vernon Hy T1 |
| 109532 | Vernon Hy T2 |
| 113098 | Deerfield 2g |
| 113099 | Deerfield 3g |
| 113100 | Deerfield G4 |
| 113101 | Deerfield G5 |
| 113102 | Fife Brook |
| 113104 | Sherman Hyd |
| 113123 | Hoosac Clr1 |
| 113125 | Hoosac Clr2 |
| 113096 | Bearswamp G1 |
| 913096 | Bearswamp P1 |
| 113097 | Bearswamp G2 |
| 913097 | Bearswamp P2 |

- No DER generation can be redispatched between contingencies to eliminate 69 kV overloaded elements.
- It is assumed that involving 69 kV double circuit towers, or 69 kV breaker failures will not cause a significant adverse impact outside the local area, and therefore were not tested.
- Hydro Generation that is defined as “Daily Cycle Pondage” or “Weekly Cycle” in the CELT report can be ramped up to nameplate capability, according to the ISO-NE Planning Technical Guide, between and contingencies to prevent post contingency thermal overloads or voltage violations. However, this generation can’t be assumed to ramp up between contingencies post Group 3, if ramping up solves voltage or thermal problems that did not exist prior to Group 3 going in-service (Per ISO-NE PP5-6 document, section 3.4: “No Increase in Conditional Dependence”).

Table 5 - Hydro Generation Available to Ramp Up between Contingencies

| RESOURCE NAME | GEN TYPE ID | PRIM FUEL TYPE | FUEL GEN TYPE DESC | STATE | RSP AREA | NAMEPLATE (MW) | WINTER SCC (MW) Jan 1, 2019 | ACTUAL WINTER PEAK SCC (MW) Jan 21, 2019 | EXPECTED SUMMER PEAK SCC (MW) JUL 1, 2019 |
|-------------------------|-------------|----------------|-------------------------------|-------|----------|----------------|-----------------------------|--|---|
| BELLOWS FALLS | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | VT | VT | 45.900 | 47.216 | 47.216 | 47.216 |
| COBBLE MOUNTAIN | HW | WAT | HYDRO (WEEKLY CYCLE) | MA | WMA | 23.100 | 27.431 | 27.431 | 31.989 |
| DEERFIELD 5 | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | MA | WMA | 17.550 | 13.990 | 13.990 | 13.965 |
| HARRIMAN | HW | WAT | HYDRO (WEEKLY CYCLE) | VT | WMA | 33.600 | 38.471 | 38.471 | 40.798 |
| JACKMAN | HW | WAT | HYDRO (WEEKLY CYCLE) | NH | NH | 3.200 | 3.459 | 3.459 | 3.600 |
| DEERFIELD 2 LWR DRFIELD | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | MA | WMA | 9.600 | 18.667 | 18.667 | 18.580 |
| SEARSBURG | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | VT | WMA | 4.500 | 4.567 | 4.567 | 4.451 |
| SHERMAN | HW | WAT | HYDRO (WEEKLY CYCLE) | MA | WMA | 8.100 | 6.220 | 6.220 | 6.154 |
| VERNON | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | VT | WMA | 34.560 | 32.000 | 32.000 | 32.000 |
| WILDER | HW | WAT | HYDRO (WEEKLY CYCLE) | VT | VT | 35.640 | 40.674 | 40.674 | 40.920 |
| CABOT TURNERS FALLS | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | MA | WMA | 61.920 | 61.800 | 61.800 | 61.800 |
| CABOT TURNERS FALLS | HDP | WAT | HYDRO (DAILY CYCLE - PONDAGE) | MA | WMA | 6.400 | 6.400 | 6.400 | 6.400 |

- Pumped Storage Generation in the study area (Northfield and Bear Swamp) can be ramped up to 1/2 nameplate capability (two units at Northfield and 1 unit at Bear Swamp) between [REDACTED] and [REDACTED] contingencies to prevent post [REDACTED] contingency thermal overloads or voltage violations. Note that this can only be assumed if the units are off or in generating mode in the base case [REDACTED]. If units are in pumping mode in the base case, it cannot be assumed that units can be ramped up into generating mode between contingencies.
- “Smart Capacitor” Control Additions in Western Massachusetts, required for the addition of the Group 1 DER interconnections, were assumed in-service for the Group 3 analysis. These “smart capacitor” controls automatically switch off distribution feeder capacitors during light load and minimum load conditions. These “smart capacitor” automation schemes are itemized in the following table.

Table 6 - “Smart Capacitor” Control Additions in Western Massachusetts

| Substation Bus | |
|---------------------|--|
| E Winchendon1 13.8 | |
| Crystal Lk1 13.8 | |
| Crystal Lk2 13.8 | |
| E Wstmstr T1 13.8 | |
| E Wstmstr T2 13.8 | |
| E Longmeadow 1 13.2 | |
| N Hampden T1 13.2 | |
| Palmer 13.2 | |
| Wilbraham 13.2 | |
| Lashaway 13.2 | |
| W Charlton 13.2 | |
| Litl Rest Rd 13.2 | |
| Thorndike 13.2 | |
| Treasure Vly 13.8 | |
| Chesnut HI T1 13.8 | |
| Chesnut HI T2 13.8 | |
| Total | |

Presently, in the existing system, the feeder capacitors listed in the preceding table are fixed capacitors; meaning that they are not switched automatically, and are in service all the time unless switched out manually in the field. After the automatic switching schemes are installed, these feeder capacitors will be switched out automatically if the feeder loading becomes less than 45% of peak feeder load. From a loadflow perspective, switching out these capacitors during light load and minimum load conditions is modeled by placing an equivalent amount of [REDACTED] lagging load at each the substation busses listed in the table. These smart capacitor controls will be installed before Group 1 of the DER cluster goes into service. The new smart capacitors will have radios for status monitoring and control. The system operators will have the ability to put the capacitors in manual operation to either open or close as needed.

- H-134 115 kV project (RSP #951) (E Winchendon to Otter River) not in-service (PPA withdrawn)
- The Ware 69 kV breaker addition project, completing the O-15N 69 kV bay, as required for interconnection of Group 2 DER of the Western MA cluster, assumed in-service.
- New Stafford St 115/13.8 kV substation in Leicester MA, which will sectionalize the A-127, B-128 and Z-126 115 kV lines near the existing Tower 510 structure, assumed in-service.
- Reconductor of A-1/B-2 69 kV lines with 795 ACSS scheduled for 2027 in-service date. Since the Group 3 DER is scheduled to be in-service between 2022 and 2025, the reconductor of A-1/B-2 was not included in the base cases for this study.
- All the transmission and generation projects with approved PPA’s were included in the base cases for this study. Additionally, the following relevant generators in the ISO-NE Interconnection Queue were modeled in each base case. Note that some of these projects that were withdrawn during the course of this study were placed out of service in the base cases.

- QP 660 (“Vernon Solar“ 20 MW PV unit connecting directly to D-4 69 kV line between Deerfield 4 and Vernon), withdrawn.
- QP-651 Alps Berkshire Phase Shifting Transformer Not In-Service (Withdrawn).
- QP697 (5.97 MW) and QP698 (8.04 MW), both connected at the E Winchendon 13.8 kV, in-service
- QP 797 [REDACTED] Solar – Meadow St) in-service
- QP 754 [REDACTED] Solar – connected to I-135N 115 kV line) Not In-Service (Withdrawn)
- QP 1105 ([REDACTED] Battery Storage Project – off A-127 115kV line) not-in-service (withdrawn from ISO-NE study queue)
- QP 1112 ([REDACTED] Storage Project – off B-128 115 kV line between Barre and French King substation) not-in-service (but tested as a sensitivity in study)
- QP 1031 ([REDACTED] Solar Project – off F-6W 69 kV line between Ware and Belchertown substations) not-in-service (but tested as a sensitivity in the study)
- Millbury 115 kV IEC61850 project – In-service. Project will replace the following [REDACTED] circuit breakers and associated Bushing Current Transformers (BCTs) with [REDACTED] circuit breakers:
 - B128, A127, Z126, M165, 27-302, 65-74, V174.
 - Replacing breakers 65-74 and V-174 will increase V-174 thermal rating [REDACTED]
[REDACTED]

4 STUDY CRITERIA

This analysis is conducted in accordance with the following criteria.

- NERC Transmission Planning Standards TPL-001-4, “*Transmission System Planning Performance Requirements*”,
- [REDACTED]
- ISO New England Planning Procedure #3 (PP3) – “*Reliability Standards for the New England Area Bulk Power System*”.
- ISO New England Planning Procedure #5 (PP5) – “*Proposed Plan Application Procedure*”.
- National Grid Transmission Group Procedure (TGP) #28 – “*Transmission Planning Guide for the National Grid USA Service Company*”.

5 STEADY STATE ANALYSIS

The following tables identify the steady state voltage criteria that were applied in the study:

Table 7 - Steady State Voltage Limits

| Facility Owner | Voltage Level | Bus Voltage Limits (Per-Unit) | |
|----------------|------------------|-------------------------------|---|
| | | Pre-Contingency | Post-Contingency |
| National Grid | 230 kV and above | 0.98 to 1.05 | 0.95 to 1.05 |
| | 115 kV and below | 0.95 to 1.05 | 0.90 to 1.05 ⁷ |
| Eversource | 115 kV and above | 0.95 to 1.05 | 0.90 to 1.05 (before system adjustments) 0.95 to 1.05 (after system adjustments) |
| GMP | 115 kV and below | 0.95 to 1.05 | 0.90 to 1.10 |
| VELCO | 230 kV and above | 0.98 to 1.05 | 0.95 to 1.05 |
| | 115 kV and below | 0.95 to 1.05 | 0.95 to 1.05 |

Table 8 - Maximum Percent Voltage Variation at Delivery Points

| CONDITION | 345 & 230 kV (%) | 115 kV ¹ & Below (%) |
|--|------------------|---------------------------------|
| Post Contingency & Automatic Actions | 5.0 | 10.0 |
| Switching of Reactive Sources or Motor Starts (All elements in service) | 2.0 * | 2.5 * |
| Switching of Reactive Sources or Motor Starts (One element out of service) | 4.0 * | 5.0 * |

* These limits are maximums which do not include frequency of operation. Actual limits were considered on a case-by-case basis and will include consideration of frequency of operation and impact on customer service in the area.

Notes on two preceding Tables:

- Voltages apply to facilities which are still in-service post-contingency.
- Site specific operating restrictions may override these ranges.
- These limits do not apply to automatic voltage regulation settings which may be more stringent.

⁷ National Grid Buses that are part of the bulk power system, and other buses deemed critical by Network Operations, shall meet requirements for 345 kV and 230 kV buses

The following table identifies the thermal criteria that is applied in the study.

Table 9 - Thermal Criteria Applied in Study

| SYSTEM CONDITION | TIME FRAME | MAXIMUM ALLOWABLE FACILITY LOADING |
|-----------------------------------|---|------------------------------------|
| Pre-contingency (All lines in) | Continuous | Normal Rating |
| Post-contingency | Less than 15 minutes after contingency occurs | STE Rating |
| | More than 15 minutes after contingency occurs | LTE Rating |

5.1 Steady State Solution Parameters

The steady state analysis is performed with pre-contingency solution parameters that allowed adjustment of load tap-changing transformers (LTCs), static VAR devices (SVDs including automatically switched capacitors. Post-contingency solution parameters were locked, and the area interchange control is disabled. The following table shows the pre- and post-contingency solution parameters that were used in this study.

Table 10 - Steady State Study Solution Parameters

| Case | Area Interchange | Transformer LTCs | Phase Angle Regulators | Switched Shunts |
|------------------|------------------|------------------|------------------------|-----------------|
| Base | Disabled | Stepping | Locked | Regulating |
| Post Contingency | Disabled | Locked | Locked | Locked |

5.2 Steady State Base Case Development

In order to investigate the impact of the proposed projects to the New England transmission system, a total of seven base cases were developed representing various load levels and interface transfer levels.

Study Year Tested

Since Group 3 of the DER will be installed by 2025, the year 2025 ISO-NE base cases, released in September 2020, were used for the steady state assessment.

Load Levels Tested

Four load levels were tested for steady state analysis. These cases are based on the loads contained in the CELT 2020 forecast.

1. Summer Peak Load
2. Shoulder Peak Load
3. Light Load
4. Minimum Load (8000 MW)

Interface Transfer Levels Tested

For each of the three load levels – Summer Peak Load, Shoulder Peak Load and Light Load, two base cases were developed for steady state testing:

1. High East to West Stress (3500 MW), with High NE-NY transfers (1200 MW), High Sandy Pond HVDC Import
2. High West to East Stress (3000 MW), with High NY-NE transfers (1600 MW), Low Sandy Pond HVDC Import

For Minimum Load level, one base case is developed for steady state testing.

The following table summarizes the interface levels and generation dispatches for the steady state base cases prior to the dispatch of Group 1,2 and 3 DER in the cases. More detailed case summaries are included in Appendix A.

To test the impact of the DER, both Group 1, 2 and 3 DER were added to each case and dispatched against Millstone 2 in Connecticut.

Table 11 - Steady State Base Case Summaries (before dispatching Group 1, 2, and 3 DER)

| Base Case Load Flows (MW) | | | | | | | |
|---|------------------|------------------|--------------------|-----------|-----------------|-----------|---------------|
| Name | 25pk-ew-100%-PV* | 25pk-we-100%-PV* | 25sh-ew+pump | 25sh-we | 25ll-ew+pump | 25ll-we | Min-load |
| Year/Load Level | 2025 Summer peak | | 2025 Shoulder peak | | 2025 Light Load | | 2025 Min Load |
| Bias | East-West | West-East | East-West | West-East | East-West | West-East | |
| Total Load | 25697 | | 18066 | | 12518 | | 8901 |
| Scaling Load | 31252 | | 16673 | | 11412 | | 7858 |
| Non-Scaling Load | 556 | | 556 | | 556 | | 556 |
| DR passive | 0 | | 0 | | 0 | | 0 |
| DR active | 0 | | 0 | | 0 | | 0 |
| EE | -4756 | | 0 | | 0 | | 0 |
| Cat 2 and 3 PV | -2089 | | 0 | | 0 | | 0 |
| NON CELT MFG LOAD | 301 | | 301 | | 301 | | 301 |
| New England Transmission Interface Transfers (MW) | | | | | | | |
| Sandy Pd HVDC Import | 2000 | 1000 | 2000 | 1000 | 2000 | 1000 | 0 |
| E-W | 3512 | -2996 | 3506 | -3036 | 3543 | -3002 | 65 |
| NY-NE | -1231 | 1600 | -1220 | 1599 | -1204 | 1602 | -34 |
| North-South | 4395 | 2212 | 3100 | 2841 | 3078 | 1584 | 2467 |
| CT Export | -1190 | -571 | -64 | -163 | -763 | 336 | 165 |
| Area Generation (MW) | | | | | | | |
| Northfield (MA) – 1180 MW (Max) | 0 | 1180 | -1100 | 1180.0 | -1100 | 0 | 0 |
| Bear Swamp 666 MW (Max) | 0 | 666 | -666 | 666 | -666 | 0 | 0 |
| Altresco (MA) – 164 MW (Max) | 0 | 164 | 73 | 164 | 164 | 164 | 0 |
| Cabot Hydro (MA) – 65 MW (Max) | 11 (minimum) | 65 | 11 (minimum) | 65 | 11 (minimum) | 65 | 11 (minimum) |
| Harriman Hydro (VT) – 41 MW (Max) | 5 (minimum) | 41 | 5 (minimum) | 41 | 5 (minimum) | 41 | 5 (minimum) |
| Vernon Hydro (VT) – 32 MW (Max) | 5 (minimum) | 32 | 5 (minimum) | 32 | 5 (minimum) | 32 | 5 (minimum) |
| Deerfield Hydro 2+3 +4 (20 MW Max) | 5 (minimum) | 20 | 5 (minimum) | 20 | 5 (minimum) | 20 | 5 (minimum) |
| Harrington St Solar (10 MW Max) | 10 | 10 | 0 | 10 | 10 | 10 | 10 |
| Warren Solar (Little Rest Rd) (14 MW Max) | 14 | 14 | 0 | 14 | 14 | 14 | 14 |
| Treasure Valley Solar (16 Max) | 16 | 16 | 0 | 16 | 16 | 16 | 16 |
| Millennium | 0 | 360 | 361 | 0 | 361 | 360 | 0 |
| Stony Brook | 0 | 483 | 0 | 483 | 483 | 483 | 0 |
| Bellows Falls | 49 | 49 | 0 | 49 | 0 | 0 | 0 |
| QP697&QP698 (14MW PV at E. Winchendon) | 14 | 14 | 0 | 14 | 14 | 14 | 14 |

*Per the direction provided by ISO-NE, all existing PV in western MA (zone 41), modeled in peak load base case was scaled up from 26% output to 100% output. This PV was modeled as negative load (with “PD” and “PV” load identifiers) in the peak load cases. Note that the negative load with “PD” identifiers includes all existing PV less than 1 MW, as well as all future forecasted PV greater than 1 MW but less than 5 MW which does not have location based data associated with it. To avoid double counting of the “PD” load that includes the future forecasted PV between 1 and 5 MW, this portion of the “PD” was stripped out of the peak load base cases. The percent of “PD” load that includes the future forecasted PV for the Western MA zone 41 is 41.9%, per ISO-NE.

Sensitivity bases cases were also developed at peak load, with all DER in the study area at 26% output (of nameplate). The following tables summarize the interface levels and generation dispatches for the steady state base cases. Again, to test the impact of the DER, Group 1, 2 and 3 DER were added to each case and dispatched against Millstone 2 in Connecticut.

**Table 12 - Steady State Base Case Summaries: Sensitivity to DER = 26% Output
(Prior to dispatching Group 1, 2, and 3 DER)**

| Base Case Load Flows (MW) | | |
|---|------------------|-------------|
| Name | 25pk-ew-26% | 25pk-we-26% |
| Year/Load Level | 2025 Summer peak | |
| Bias | East-West | West-East |
| Total Load | 26338 | 26282 |
| Total Losses | 966 | 683 |
| Total Generation | 27670 | 24419 |
| Scaling Load | 31227 | |
| Non-Scaling Load | 556 | |
| DR passive | 0 | |
| DR active | 0 | |
| EE | -4756 | |
| Station Service | 678 | 621 |
| NON CELT LOAD | 301 | |
| New England Transmission Interface Transfers (MW) | | |
| Sandy Pd HVDC Import | 2000 | 1000 |
| E-W | 3521 | -2987 |
| NY-NE | -1188 | 1641 |
| North-South | 4506 | 2321 |
| CT Export | -742 | -97 |
| Area Generation (MW) | | |
| Northfield (MA) – 1180 MW (Max) | 0 | 1180 |
| Bear Swamp 666 MW (Max) | 0 | 666 |
| Altresco (MA) – 164 MW (Max) | 0 | 164 |
| Cabot Hydro (MA) – 65 MW (Max) | 11* (minimum) | 65 |
| Harriman Hydro (VT) – 41 MW (Max) | 5* (minimum) | 41 |
| Vernon Hydro (VT) – 32 MW (Max) | 5* (minimum) | 32 |
| Deerfield Hydro 2+3 +4 (20 MW Max) | 5* (minimum) | 20 |
| Harrington St Solar (10 MW Max) | 10 | 10 |
| Warren Solar (Little Rest Rd) (14 MW Max) | 14 | 14 |
| Treasure Valley Solar (16 Max) | 16 | 16 |
| Millenium | 0 | 360 |
| Stony Brook | 0 | 483 |
| Bellows Fall | 49 | 49 |
| QP697&QP698 (14MW PV at E. Winchendon) | 14 | 14 |

5.3 Study Matrix for Steady State Analysis

To test the impact of the DER, Group 1,2 and 3 DER were added to each case, according to the following table, and dispatched against Millstone 2 in Connecticut. Dispatching the DER against Millstone 2 will maintain the same East-West, and NY-NE transfer levels, compared to the pre-DER base cases.

Table 13 – Proposed Study Matrix for Steady State Analysis

| | | Group 3 DER | | Group 1 and 2 DER | Pre-Group 1 and 2 DER | FERC BESS projects under Study | |
|--------------------|-----------|------------------|--|--|--------------------------------------|--|--|
| Load Level | Bias | BESS output | PV output | PV output | PV output | | Comments |
| Peak Summer load | E-W | 100% | 100% | 100% | 100% | Sensitivity analysis was conducted for ██████████ (QP1031) and ██████████ (QP1112) | |
| | W-E | discharging | | | | | |
| | E-W | 100% Charging | 26% | 26% | 26% | | |
| | W-E | | | | | | |
| | | | | | | | |
| Shoulder Peak Load | E-W +pump | 100% Charging | 0% (peak load night/morning - before 8am) | 0% (peak load night - before 8am) | 0% (peak load night - before 8am) | | This case represents a peak load night. BESS could be charging (7am) before Bear Swamp Pumps shut off. PV assumed to 0 MW in case. |
| | W-E | 100% discharging | 100% (no pump case (day)) | 100% for PV 5 MW and above. 100% for PV under 5 MW | 0% | | |
| | | | | | | | |
| Light Load | E-W +pump | 100% discharging | 100% | 100% for PV 5 MW and above. 100% for PV under 5 MW | 0% | | |
| | W-E | | | | | | |
| | | | | | 0% | | |
| Min Load | none | 100% discharging | 100% | 100% for PV 5 MW and above. 100% for PV under 5 MW | 0% | | |

5.4 Steady State Contingency Analysis

N-1 and N-1-1 contingency conditions were tested in steady state analysis on the load flow base cases with and without the new DER added to the cases.

5.4.1 N-1 Contingency List

The N-1 Contingency list is shown in the table below.

Table 14 - N-1 Steady State Contingency List

| CONTINGENCY NAME | kV | DESCRIPTION |
|---|---------|---|
| HVDC Facilities | | |
| Sandy Pond HVDC Phase II | - | Sandy Pond HVDC Converter – 2000 MW Maximum |
| 345 kV Transmission Lines | | |
| 301/302 | 345 | Millbury – Carpenter Hill – Ludlow |
| 308 | 345 | Wachusett – Millbury |
| 312 | 345 | Berkshire – Northfield (Post Alps-Berkshire ETU) |
| 393 | 345 | Alps – Berkshire (Post Alps-Berkshire ETU) |
| 313 | 345 | Wachusett – Millbury |
| 314 | 345 | Sandy Pond – Wachusett |
| 326 | 345 | Scobie – Sandy Pond |
| 320 | 345 | Lake Rd – Card St |
| 343 | 345 | Sandy Pond – Wachusett |
| 354 | 345 | Northfield – Ludlow |
| 367 | 345 | Amherst – Fitzwilliam |
| 3195 | 345 | Amherst – Eagle |
| 380 | 345 | Eagle – Scobie Pd |
| 368 | 345 | Manchester – Card St |
| 379 | 345 | Vernon – Fitzwilliam |
| 381 | 345 | Vernon – Northfield |
| 398 | 345 | Long Mt – Pleasant Valley (NY) |
| 3340 | 345 | Vernon – Vermont Yankee |
| 3381 | 345 | Vernon – Vermont Yankee |
| 3271 | 345 | Lake Rd – Card St |
| 330 | 345 | Lake Rd – Card St |
| 3348 | 345 | Lake Rd – Killingly |
| 341 | 345 | Lake Rd – W Farnum |
| 368 | 345 | Card St - Manchester |
| 345 kV Transformers | | |
| Wachusett T5 | 345/115 | Wachusett Transformer #5 |
| Wachusett T6 | 345/115 | Wachusett Transformer #6 |
| Wachusett T7 | 345/115 | Wachusett Transformer #7 |
| Fitzwilliam T1 | 345/115 | Fitzwilliam Transformer #1 |
| Ludlow T2 | 345/115 | Ludlow Transformer #2 |
| Ludlow T3 | 345/115 | Ludlow Transformer #3 |
| Northfield T1 | 345/115 | Northfield Transformer #1 (post Pittsfield-Greenfield upgrades) |
| Berkshire T1 | 345/115 | Berkshire Transformer #1 |
| Carpenter Hill T1 | 345/115 | Carpenter Hill Transformer #1 |
| Agawam T1 | 345/115 | Agawam T1 |
| Agawam T2 | 345/115 | Agawam T2 |
| 345 kV Line End Open Contingencies | | |
| 301 Millbury | 345 | Millbury – Carpenter Hill |
| 302 Ludlow | 345 | Ludlow – Carpenter Hill |
| 312 Northfield | 345 | Northfield – Berkshire |
| 345 kV Breaker Open Contingencies | | |
| 393 Alps | 345 | Berkshire - Alps |
| 345 kV Breaker Failures | | |
| Fitzwilliam 3791 BF | 345 | 379 + Fitz T1 |
| Fitzwilliam 671 BF | 345 | 367 + Fitz T1 |

| CONTINGENCY NAME | kV | DESCRIPTION |
|----------------------------------|---------|--|
| Wachusett 7T BF | 345 | 308 + Wachusett T7 |
| Wachusett 6T BF | 345 | 313 + Wachusett T6 |
| Wachusett43-6T BF | 345 | 343 + Wachusett T6 |
| Wachusett 14-7T BF | 345 | 314 + Wachusett T7 |
| Ludlow 1T BF | 345 | 334 + Ludlow T2 |
| Ludlow 2T BF | 345 | 334 + Ludlow T3 |
| Ludlow 3T BF | 345 | Ludlow T3 |
| Ludlow 4T BF | 345 | 354 + Ludlow T2 |
| Ludlow 5T BF3t19 | 345 | 3196 + 354 |
| Ludlow 6T BF | 345 | 3196 |
| Ludlow 7T BF | 345 | 301/302 + Ludlow T2+ Carpenter Hill Auto |
| Ludlow 8T BF | 345 | 3419 + 301/302 + Ludlow T2+ Carpenter Hill Auto |
| Ludlow 9T BF | 345 | 3419 |
| Millbury 308+302 BF | 345 | 301/302 + 308 |
| Northfield 2T BF | 345 | 312 + Northfield G1 + G2 (post Pittsfield-Greenfield upgrades) |
| Northfield 5T BF | 345 | 354 + Northfield G3 + G4 (post Pittsfield-Greenfield upgrades) |
| Vernon 3TB4-B1 BF | 345 | 381 + Vernon Reactor |
| Vernon 3TB3-B1 BF | 345 | 379 + 3381 |
| Vernon 3TB1-B1 BF | 345 | 3320 + 3340 |
| Vernon 3TB2-B1 BF | 345 | 340 + Vernon T1 |
| Vermont Yankee 1T | 345 | Vermont Yankee GSU |
| Vermont Yankee 381 | 345 | 3381 + Vermont Yankee Auto |
| Vermont Yankee 81-1T | 345 | 3381 + Vermont Yankee GSU |
| Vermont Yankee 79-40 | 345 | 3340 + Vermont Yankee Auto |
| 345 kV Double Ckt Towers | | |
| - | - | - |
| 230 kV Transmission Lines | | |
| E-205E | 230 | Bear Swamp – Pratts Jct. |
| E-205W | 230 | Bear Swamp – Eastover Rd (NY) |
| 38 | 230 | Rotterdam (NY) – Eastover Rd (NY) |
| 230 kV Double Ckt Towers | | |
| - | - | - |
| 230/115 kV Transformers | | |
| Bear Swamp T4 | 230/115 | Bear Swamp Transformer #4 |
| Bear Swamp T5 | 230/115 | Bear Swamp Transformer #5 |
| PrattsJct T8 + T8A | 230/115 | PrattsJct Transformer #8 + 8A |
| Eastover Rd T1 | 230/115 | Eastover Rd Transformer #1 |
| Eastover Rd T2 | 230/115 | Eastover Rd Transformer #2 |
| 230 kV Breaker Failures | | |
| Bear Swamp 2205E BF | 230 | Bear Swamp G2 + T4 (230-115 kV) + E-205E |
| Bear Swamp 2205W BF | 230 | Bear Swamp G2 + T4 (230-115 kV) + E-205W |
| Bear Swamp 1205E BF | 230 | Bear Swamp G1 + T5 (230-115 kV) + E-205E + 115 kV Cap |
| Bear Swamp 1205W BF | 230 | Bear Swamp G1 + T5 (230-115 kV) + E-205W + 115 kV Cap |
| Eastover Rd RE205 BF | 230 | E-205W + Eastover Rd T1 |
| Eastover Rd RE215 BF | 230 | E-205W + Eastover Rd T2 |
| Eastover Rd R38 BF | 230 | 38 + Eastover Rd T1 |
| Eastover Rd R48 BF | 230 | 38 + Eastover Rd T2 |
| 115 kV Transmission Lines | | |
| 1242 | 115 | Montague – Berkshire |
| 1361 | 115 | Montague – Cumberland (post Pittsfield-Greenfield upgrades) |
| 1231 | 115 | Berkshire – Cumberland |
| 1551 | 115 | Doreen – Berkshire |
| 1662 | 115 | Doreen – Berkshire |
| PV20 | 115 | Plattsburg – South Hero |
| K6 | 115 | Bennington – Hoosick (NY) |
| K7 | 115 | Whitehall – Bliss Ville |
| A-127E | 115 | Millbury- Webster St – Erving (post Erving substation) |
| A-127W | 115 | Erving – Harriman (post Erving substation) |
| B-128 | 115 | Harriman – Millbury |
| E-131 | 115 | Bear Swamp – Harriman – Adams |
| F-132 | 115 | Adams – Doreen |
| I-135 | 115 | Fitzwilliam – Flagg Pd |
| I-135S | 115 | Flagg Pd – PrattsJct |
| J-136S | 115 | Flagg Pd – Litchfield Tap – PrattsJct |
| J-136N | 115 | Bellows Falls – Flagg Pd |

| CONTINGENCY NAME | kV | DESCRIPTION |
|---------------------------------|--------|---|
| O-141 | 115 | Greendale – Nashua St |
| O-141N | 115 | PrattsJct – Wachusett |
| O-141S | 115 | Nashua St – Millbury |
| O-141W | 115 | Wachusett– Greendale |
| P-142 | 115 | W Boylston – Rolfe Ave |
| P-142N | 115 | PrattsJct – Wachusett |
| P-142S | 115 | Rolfe Ave – Millbury |
| P142W | 115 | Wachusett – W Boylston |
| Q-117 | 115 | Adams – Bennington |
| R-170 | 115 | Palmer – W Hampden |
| 1205 | 115 | W Hampden - Ludlow |
| 1976 | 115 | W Hampden - Scitico |
| S-197 | 115 | Bear Swamp – Deerfield |
| V-174W | 115 | Carpenter Hill – N Oxford |
| V-174 | 115 | N Oxford – Millbury |
| W-175 | 115 | Carpenter Hill – Palmer |
| X-176 | 115 | Palmer – Ludlow |
| Y-177 | 115 | Harriman – Montague (NU) |
| Z-126 | 115 | Millbury – Tower 510 – Webster St |
| 115 kV Double Ckt Towers | | |
| 1161+1211 DCT | 115 | 1161 + 1211 + 1662 |
| 1231+1242 DCT | 115 | 1231 + 1242 |
| 1551+1662 DCT | 115 | 1551 + 1662 + 1211 |
| 1715+1816 DCT | 115 | 1715 + 1816 + Altresco Gen |
| A127E+B128 DCT | 115 | A-127E + B-128 (Millbury – Erving) (post Erving substation) |
| A127W+B128 DCT | 115 | A-127W + B-128 (Erving – Harriman) (post Erving substation) |
| 141W+142 DCT | 115 | O-141W + P-142 |
| O141S+P142 DCT | 115 | O-141S + P-142 |
| O141N+P142N DCT | 115 | O-141N + P-142N |
| O141S+142S DCT | 115 | O-141S + P-142S |
| O141W+P142W DCT | 115 | O-141W + P-142W |
| I135S+J136S DCT | 115 | I-135S + J-136S |
| I135N+J136N DCT | | I-135N + J-136N |
| I135+J136N DCT | | I-135 + J-136N |
| 115/69 kV Transformers | | |
| Millbury T1 | 115/69 | Millbury Transformer #1 (56 MVA) |
| Millbury T2 | 115/69 | Millbury Transformer #2 (56 MVA) |
| Millbury T3 | 115/69 | Millbury Transformer #3 (45 MVA) + 63 Mvar Cap Bank |
| Pratts Jct T5 + T6 + T7 | 115/69 | PrattsJct Transformer bank #1 |
| PrattsJct T3+T4 | 115/69 | PrattsJct Transformer bank #2 |
| Deerfield 4 T3 + T4 | 115/69 | Deerfield4 transformer #3 + T4 |
| Adams Autotransformer | 115/69 | Adams Autotransformer |
| Bennington T69 | 115/69 | Bennington VT 115-69 kV transformer |
| Harriman Autotransformer | 115/69 | Harriman Autotransformer |
| Palmer Transformer bank #1 | 115/69 | Palmer T3 + T5 |
| Palmer Transformer bank #1 | 115/69 | Palmer T4 + T6 |
| W Hampden T1 | 115-69 | West Hampden T1 |
| 115 kV Breaker Failures | | |
| Adams 731 BF | 115 | E-131 + Q-117 (Post Adams Upgrade) |
| Adams 217 BF | 115 | F-132 + Q-117 (Post Adams Upgrade) |
| Adams T3T BF | 115 | F-132 + Adams Auto (Post Adams Upgrade) |
| Adams T5T BF | 115 | E-131 + Adams Auto (Post Adams Upgrade) |
| Bear Swamp 131 BF | 115 | E-131 + Bear Swamp T4 + Bear Swamp GSU #1 |
| Bear Swamp 197 BF | 115 | S-197 + Bear Swamp T4 + Bear Swamp GSU #1 |
| Bear Swamp T31 BF | 115 | E-131 + Bear Swamp Fut Xfmr + Bear Swamp 115 kV Cap + Bear Swamp GSU #2 (Post Bear Swamp Upgrade) |
| Bear Swamp T97 BF | 115 | S-197 + Bear Swamp Fut Xfmr + Bear Swamp 115 kV Cap + Bear Swamp GSU #2 (Post Bear Swamp Upgrade) |
| Bennington K4 BF | 115 | Q-117 + Bennington 115 kV Cap #1 |
| Bennington KT1 BF | 115 | Bennington Auto + Bennington 115 kV Cap #2 |
| Berkshire 12T BF | 115 | 1551 + Berkshire T2 |
| Berkshire 13T BF | 115 | 1551 + 1231 |
| Berkshire 16T BF | 115 | 1662 +1242 |
| Doreen 6T BF | 115 | 1161 + 1662 |
| Doreen 7T BF | 115 | 1211 + 1662 |
| Doreen 8T BF | 115 | 1211 + 1551 |
| Doreen 9T BF | 115 | 1551 + 1816 |

| CONTINGENCY NAME | kV | DESCRIPTION |
|---|-----|--|
| Doreen 12T BF | 115 | 1715 + F-132 |
| Erving A BF | 115 | A-127W + A-127E open ended + Northfield T1 |
| Erving B BF | 115 | A-127E + A-127W open ended + Northfield T1 |
| Erving C BF | 115 | A-127E + A-127W + Northfield T1 |
| Harriman A127 BF | 115 | A-127W + B-128 open ended |
| Harriman B128 BF | 115 | A-127W open ended + B-128 |
| Harriman E131 BF | 115 | E-131 + Y177 open ended + Harriman G1 + G2 +G3 |
| Harriman Y177 BF | 115 | E-131 open ended + Y177 + Harriman G1 + G2 +G3 |
| Harriman TIE BF | 115 | A-127W open ended + B-128 open ended + E-131 open ended + Y177 open ended + Harriman G1 + G2 +G3 |
| Montague 1T BF | 115 | 1632 + Cabot Gen |
| Montague 3T BF | 115 | 1044 + Y-177 open ended |
| Montague 7T BF | 115 | 1361 + A-127W open ended |
| Montague 8T BF | 115 | 1361 + 1242 |
| Montague 10T BF | 115 | 1242 + Cabot Gen |
| PrattsJct O141 BF | 115 | Pratts T3 + T4 115-69 kV autos + O-141N + Pratts 63 MVAR capacitor |
| PrattsJct 801 BF | 115 | Pratts T3 + T4 115-69 kV autos + E-205E + Pratts 63 MVAR capacitor |
| PrattsJct I135 BF | 115 | Pratts T3 + T4 115-69 kV autos + I-135S + Pratts 63 MVAR capacitor |
| PrattsJct 1110 BF | 115 | Pratts T3 + T4 115-69 kV autos + Pratts 63 MVAR capacitor |
| PrattsJct P142 BF | 115 | Pratts T3 + T4 115-69 kV autos + P-142N + Pratts 63 MVAR capacitor |
| PrattsJct 802 BF | 115 | Pratts T5 + T6 + T7 115-69 kV autos + E-205E + J-136 (PJ – Litch Tap) |
| PrattsJct L138 BF | 115 | Pratts T5 + T6 + T7 115-69 kV autos + L-138 + J-136 (PJ – Litch Tap) |
| PrattsJct K137 BF | 115 | Pratts T5 + T6 + T7 115-69 kV autos + K-137 + J-136 (PJ – Litch Tap) |
| PrattsJct J136 BF | 115 | Pratts T5 + T6 + T7 115-69 kV autos + J-136S |
| PrattsJct 2110 BF | 115 | Pratts T5 + T6 + T7 115-69 kV autos + J-136 (PJ – Litch Tap) |
| PrattsJct 38-42 BF | 115 | L-138W + P-142N |
| PrattsJct 37-41 BF | 115 | K-137W + O-141N |
| 115 kV Capacitor Banks | | |
| Bear Swamp Cap #1 | 115 | Bear Swamp 63 Mvar Cap Bank |
| Bear Swamp Cap #2 | 115 | Bear Swamp 63 Mvar Cap Bank |
| 115 kV Line-End Open Contingencies | | |
| 1242 Mont-open | 115 | Montague – Berkshire |
| 1242 Berk-open | 115 | Montague – Berkshire |
| 1231 Berk-open | 115 | Berkshire – Cumberland |
| 1231 Cumb-open | 115 | Berkshire – Cumberland |
| A-127 Millb-open | 115 | A-127 (Millbury – Tower 510) |
| B-128 Millb-open | 115 | B-128 (Millbury – Tower 510) |
| I135 Flagg-open | 115 | I-135 (Flagg Pd – Chinook) |
| I-135 Fitz-open | 115 | I-135 (Fitzwilliam – Chinook) |
| J136S Flagg-open | 115 | J-136S (Flagg Pd – Litchfield St Tap) |
| O141N Wach-open | 115 | O-141N (Wachusett – Sterling) |
| O141N Pratts-open | 115 | O-141N (PrattsJct – Sterling) |
| P142N Wach-open | 115 | P-142N (Wachusett – Sterling) |
| P142N Pratts-open | 115 | P-142N (Pratts Jct – Sterling) |
| P142S Milb-open | 115 | P-142S (Millbury – Wyman Gordon) |
| P142S Bloom-open | 115 | P-142S (Rolfe Ave. – Bloomingdale Tap) |
| P142S Rolfe-open | 115 | P-142S (Rolfe Ave – Bloomingdale Tap) |
| E131 Bear-open | 115 | E-131 (Bear Swamp – Bear Swamp Jct) |
| E131 Adams-open | 115 | E-131 (Adams – Bear Swamp Jct) |
| F132 Doreen-open | 115 | F-132 (Doreen – Partridge) |
| W-175 Carp-open | 115 | W-175 (Carpenter Hill – W Charlton) |
| W-175 Palm-open | 115 | W-175 (Palmer – Little Rest Rd) |
| X-176 Palm-open | 115 | X-176 (Palmer – Thorndike) |
| X-176 Ludlow-open | 115 | X-176 (Ludlow – Thorndike) |
| 115 kV Breaker Open Contingencies | | |
| A127W Harriman | 115 | Harriman - Cabot Jct |
| J136S Pratts | 115 | Pratts Jct – Litchfield tap |
| I135N-Bellows | 115 | Bellows Falls – Fitzwilliam Tap |
| J136N-Bellows | 115 | Bellows Falls – E Winchendon |
| E131-harriman | 115 | Harriman – Bear Swamp Jct |
| B128-harriman | 115 | Harriman – Cabot Jct |
| Y177-harriman | 115 | Harriman – Sherman |
| Harriman T3 115 kV | 115 | Harriman T3 115 kV winding - Midpoint |
| 115 kV Bus Faults | | |

| CONTINGENCY NAME | kV | DESCRIPTION |
|--|-----|---|
| Harriman Bus #1 | 115 | A-127 open ended + B128 open ended + GSU # 1 + #2 (Post-Harriman Tie breaker) |
| Harriman Bus #2 | 115 | E-131 open ended + Y-177 open ended + T3 open ended (Post-Harriman Tie breaker) |
| Pratts Bus #1 | 115 | |
| Pratts Bus #2 | 115 | |
| 69 kV Transmission Lines | | |
| A-1 | 69 | Otter River – Chestnut Hill |
| A-1N | 69 | Chestnut Hill – Vernon |
| A-1S | 69 | PrattsJct – Otter River |
| B-2N | 69 | Park St – Vernon |
| B-2S | 69 | PrattsJct – Park St (Gardner) |
| D-4N | 69 | Vernon – QP660 |
| D-4S | 69 | QP660- Deerfield 4 |
| E-5 | 69 | Meadow St. – Ware |
| E-5D | 69 | Shutesbury – Deerfield 4 |
| E-5E | 69 | Millbury – Meadow St |
| E-5W | 69 | Ware – Shutesbury |
| F-6 | 69 | Meadow St. – Ware |
| F-6E | 69 | Millbury – Meadow St |
| F-6W | 69 | Ware – Deerfield 4 |
| J-10 | 69 | Adams – Deerfield 5 |
| M-39 | 69 | Fitch Rd – Wachusett |
| N-40 | 69 | Fitch Rd – PrattsJct |
| N-14 | 69 | Palmer – E Longmeadow |
| O-15N | 69 | Palmer – Ware |
| O-15S | 69 | W Hamden - E Longmeadow |
| Y-25N-1 | 69 | Searsburg – Searsburg Wind |
| Y-25N-2 | 69 | Bennington – Deerfield Wind |
| Y-25S | 69 | Deerfield 5 – Harriman – Searsburg |
| 69 kV Breaker Failures | | |
| Pratts A1S BF | 69 | A-1S + U-21S + N-40 + open end 69 kV side of Pratts 115/69 kV transformer bank #1 |
| Pratts B2S BF | 69 | B-2S + V-22S + open 69 kV side of Pratts 115/69 kV transformer bank #2 |
| Pratts 160 BF | 69 | Pratts 115/69 kV transformer bank #2 + Open end A-1S + N-40 + U-21S |
| Pratts 260 BF | 69 | Pratts 115/69 kV transformer bank #2 + Open end B-2S + V-22S |
| Pratts Tie BF | 69 | PrattsJct 69 kV busses #1 and #2 (open all lines and transformers at PrattsJct 69 kV) |
| Pratts U21 BF | 69 | U-21S + N-40 + open end 69 kV side of Pratts 115/69 kV transformer bank #1 + open end A-1S |
| Pratts V22 BF | 69 | V-22S + open end B-2S + open 69 kV side of Pratts 115/69 kV transformer bank #2 |
| Deerfield #4 540 | 69 | E-5D + Deerfield 69 kV bus (open end all other facilities out of Deerfield 69 kV) |
| Deerfield #4 640 | 69 | F-6W + Deerfield 69 kV bus (open end all other facilities out of Deerfield 69 kV) |
| Crystal Lake B2S BF | 69 | B-2S + Crystal Lake T1 (69/13kV) |
| Crystal Lake B2N BF | 69 | B-2N + Crystal Lake T2 (69/13kV) |
| Searsburg Y25 BF | 69 | Y-25N-1 + Y25S |
| Deerfield Wind Y25-1 BF | 69 | Searsburg Wind + Y-25N-1 + Y-25N-2 open ended |
| Deerfield Wind Y25-2 BF | 69 | Searsburg Wind + Y-25N-2 + Y-25N-1 open ended |
| Deerfield Wind Y25-Tie BF | 69 | Searsburg Wind + Y-25N-1 + Y-25N-2 |
| Adams 360 BF | 69 | Adams 115/69kV Autotransformer + J-10 |
| Chestnut Hill 230 BF | 69 | A-1N + A-1 open ended + T2 |
| Chestnut Hill 130 BF | 69 | A-1 + A-1N open ended + T1 |
| Otter River A1 BF | 69 | A-1 + A-1S open ended |
| Otter River A1S BF | 69 | A-1S + A-1 open ended |
| Harriman 3810 BF | 69 | Y-25S + Harriman G3 + Harriman 115/69kV Autotransformer |
| Vernon A1 BF | 69 | A-1N + GSU #1 |
| Vernon B2 BF | 69 | B-2N + D-4 open ended + GSU #2 |
| Vernon D4 BF | 69 | B-2N + D-4 open ended + GSU #2 |
| Vernon Tie BF | 69 | All lines (A-1N, B-2N, D-4) open ended + GSU #1 & #2 |
| Bennington Y25 BF | 69 | Y-25N-2 + Benn 115/69kV Autotransformer + Benn Cap #2 |
| 69 kV Line-End Open Contingencies | | |
| E-5E Mill-open | 69 | Millbury – Pondville |
| E-5 Meadow-open | 69 | Meadow St – Harrington St |
| E-5W Ware-open | 69 | Ware - Shutesbury |
| F-6E Mill-open | 69 | Millbury - Pondville |
| F-6 Meadow-open | 69 | Meadow St. – Lashaway |
| F-6W Ware-open | 69 | Ware – Belchertown |

| CONTINGENCY NAME | kV | DESCRIPTION |
|---|----------|---|
| 69 kV Breaker Open Contingencies | | |
| A-1 Otter River | 69 | Royalston – Otter River |
| A-1S Otter River | 69 | Otter River – E Westminster |
| A1 Chestnut Hill | 69 | Chestnut Hill – Royalston |
| A1S Pratts Jct | 69 | Pratts Jct – E Westminster |
| B2S Pratts Jct | 69 | Pratts Jct – E Westminster |
| B-2S Crystal Lake | 69 | Crystal Lake - Westminster |
| B-2N Crystal Lake | 69 | Crystal Lake – Otter River |
| E5D Deerfield 4 | 69 | Deerfield 4 – Deerfield 3 |
| F6 Meadow St | 69 | Meadow St - Lashaway |
| F6 Shutesbury | 69 | Shutesbury – Deerfield 2 |
| F6W Deerfield 4 | 69 | Deerfield 4 – Deerfield 3 |
| Harriman T3 69 kV | 69 | Harriman T3 69 kV winding - Midpoint |
| Y25 Searsburg | 69 | Searsburg North bus - Searsburg South bus |
| Y25 Deerfield 5 | 69 | Deerfield 5 – Hoosic Wind Tap |
| 69 kV Bus Faults | | |
| Pratts Bus #1 | 69 | |
| Pratts Bus #2 | 69 | |
| Vernon #1 | 69 | A-1 open ended at Vernon + GSU #1 |
| Vernon #2 | 69 | B-2 and D-4 open ended at Vernon + GSU #2 |
| Deerfield #4 | 69 | All lines open ended at Deerfield 4 (E-5, F-6, D-4) |
| 69 kV Double Ckt Towers | | |
| A1S+B2S | 69 | |
| A1S+B2N | 69 | |
| A1+B2N | 69 | |
| A1N+B2N | 69 | |
| E5E+F6E DCT | 69 | |
| E5+F6 DCT | 69 | |
| E5W+F6W DCT | 69 | |
| E5D+F6W DCT | 69 | |
| Generators/GSU | | |
| Harriman Hydro (VT) | 115/6.9 | GSU 1 |
| Harriman Hydro (VT) | 115/6.9 | GSU 2 |
| Harriman Hydro (VT) | 115/6.9 | GSU 3 |
| Cabot Hydro (MA) | 115/13.8 | Cabot GSU |
| Northfield (MA) | 345/13.8 | GSU #1 Unit 1 + Unit 2 |
| Northfield (MA) | 345/13.8 | GSU #2 Unit 3 + Unit 4 |
| Altresco (MA) | 115/13.8 | Unit 1 + Unit 2 |
| Altresco (MA) | 115/13.8 | Unit 3 + Unit 4 |
| Vernon Hydro #1 (VT) | 69/13.8 | GSU #1 |
| Vernon Hydro #2 (VT) | 69/13.8 | GSU #2 |
| Seabrook | 345 | |
| Bear Swamp G1/P1 | 230 kV | Bear Swamp Generator/Pump #1 |
| Bear Swamp G2/P2 | 230 kV | Bear Swamp Generator/Pump #2 |
| Millenium GT + ST | 115 kV | Millennium Gas Turbine + Steam Turbine Unit |

5.4.2 N-1-1 Contingency List

The following table lists the contingencies that was tested as the first line out in N-1-1 contingency analysis. In each line-out case, all contingencies described in previous section is tested as the second contingency.

Table 15 - N-1-1 Contingency List

| Initial facility out (N-1), one at a time | Second Contingency (N-1-1) |
|--|--|
| <p>Each transmission circuit (69 kV and above) tested in N-1 analysis</p> <p>Each transmission transformer (115/69 kV and above) tested in N-1 analysis</p> <p>Each Generator (connected to 69 kV and above) tested in N-1 Analysis</p> <p>Loss of Seabrook G1</p> <p>Loss of Sandy Pond HVDC Pole 1</p> <p>Loss of Sandy Pond HVDC Pole 2</p> <p>Shunt Device</p> | <p>All contingencies listed in Table 14 except:</p> <p>Non BPS* Double Circuit Towers</p> <p>Non BPS* Breaker Failures</p> <p>Non BPS* Bus sections</p> <p>Line-End-Open Contingencies</p> |

* Non BPS equipment is defined as any line or device that is not terminated at a BPS station

Steady State Results

5.4.3 N-0 Thermal and Voltage Results

N-0 Thermal Results

Simulation results indicate that addition of the Group 3 DER, incremental to the Groups 1+2 DER, results in several transmission facility overloads during all-lines-in conditions as shown in table below.

Table 16 - N-0 Thermal Overloads

| Worst case Loading at or above 100% of LTE Rating | | | | Base case |
|--|----|----------------------|-----------------|----------------------------------|
| Overloaded Facility | KV | Summer Normal Rating | Loading (% LTE) | |
| B-2 [Pratts Jct – E Westminster] (2/0 Cu O/H line) | 69 | | | 25pk-we-pv=100% + BESS discharge |
| | | | | 25sh-we_PV=100% + BESS discharge |
| | | | | 25ll-we_PV=100% + BESS discharge |
| | | | | 25sh-ew+pump PV=0% BESS Charging |
| B-2 [E Westminster - Westminster] (2/0 Cu O/H line) | 69 | | | 25pk-we-pv=100% + BESS discharge |
| | | | | 25sh-we_PV=100% + BESS discharge |
| B-2 [Westminster – Crystal Lake] (2/0 Cu O/H line) | 69 | | | 25sh-we_PV=100% + BESS discharge |

N-0 Voltage Results

No N-0 voltage violations were found for any of the conditions tested.

N-1 Thermal and Voltage Results

N-1 Thermal Results

Simulation results indicate that addition of the Group 3 DER, incremental to the Groups 1+2 DER, results in several transmission facility overloads following N-1 contingencies as shown in table below.

Table 17 - N-1 Thermal Overloads

| Worst case Loading at or above 100% of LTE Rating | | | | Base case | CONTINGENCY (Loss of) |
|--|----|---------------|--------------------|----------------------------------|--------------------------|
| Overloaded Facility | KV | LTE Rating | Loading (% LTE) | | |
| B-2 [Pratts Jct – E Westminster] (2/0 Cu O/H line) | 69 | | | 25pk-we-pv=100% + BESS discharge | |
| | | | | 25sh-we_PV=100% + BESS discharge | |
| | | | | 25ll-we_PV=100% + BESS discharge | |
| | | | | 25sh-ew+pump PV=0% BESS Charging | |
| B-2 [E Westminster - Westminster] (2/0 Cu O/H line) | 69 | | | 25sh-we_PV=100% + BESS discharge | |
| | | | | 25pk-we-pv=100% + BESS discharge | |
| | | | | 25pk-we-pv=100% + BESS discharge | |
| | | | | 25sh-we_PV=100% + BESS discharge | |
| B-2 [Westminster – Crystal Lake] (2/0 Cu O/H line) | 69 | | | 25sh-ew+pump PV=0% BESS Charging | |
| | | | | 25sh-we_PV=100% + BESS discharge | |
| | | | | 25sh-we_PV=100% + BESS discharge | |
| | | | | 25sh-we_PV=100% + BESS discharge | |
| A-1 [Otter River - Royalston] (2/0 Cu O/H line) | 69 | | | 25sh-we_PV=100% + BESS discharge | |
| | | | | 25sh-we_PV=100% + BESS discharge | |

If QP1031 [REDACTED] goes forward, the addition of Group 3 DER results in the following additional N-1 overloads.

Table 18 – Additional N-1 Thermal Overloads

(w/ [REDACTED] (QP1031) and [REDACTED] (QP1112) In-service)

| Worst case Loading at or above 100% of LTE Rating | | | | Base case | CONTINGENCY (Loss of) |
|---|----|---------------|--------------------|----------------------------------|--------------------------|
| Overloaded Facility* | KV | LTE Rating | Loading (% LTE) | | |
| E-5 [Meadow St- Leicester] (477 ACSR) | 69 | [REDACTED] | [REDACTED] | 25pk-we-pv=100% + BESS discharge | [REDACTED] |
| F-6 [Meadow St- Leicester] (477 ACSR) | 69 | [REDACTED] | [REDACTED] | 25pk-we-pv=100% + BESS discharge | |
| E-5 [Leicester - Pondville] (477 ACSR) | 69 | [REDACTED] | [REDACTED] | 25pk-we-pv=100% + BESS discharge | |
| F-6 [Leicester - Pondville] (477 ACSR) | 69 | [REDACTED] | [REDACTED] | 25pk-we-pv=100% + BESS discharge | |
| E-5 [Meadow St – Harrington St] (477 ACSR) | 69 | [REDACTED] | [REDACTED] | 25pk-we-pv=100% + BESS discharge | |

*All additional Overload facilities are due to the inclusion of QP1031 [REDACTED] only, not QP1112 [REDACTED].

N-1 Voltage Results

Simulation results indicate that the addition of the Group 3 DER (With or without QP1031 or QP 1112), results in several high and low voltage violations along the A1/B2 69 kV transmission circuits for several N-1 contingencies. These overloads are shown in the following table.

Table 19 - N-1 Voltage Violations

| BUSSES W/ VOLTAGE VIOLATIONS | | Voltage | BASE CASE | CONTINGENCY |
|------------------------------|----|---------|----------------------------------|-------------|
| Bus | KV | Pu | | (Loss of) |
| E Westminster (A1) | 69 | 1.07 | 25min pv=100% + BESS discharge | |
| | | 0.88 | 25sh-ew+pump PV=0% BESS Charging | |
| E Westminster (B2) | 69 | 1.06 | 25min pv=100% + BESS discharge | |
| Westminster (B2) | 69 | 1.06 | 25sh-we pv=100% + BESS discharge | |
| Vernon (A1/B2) | 69 | 1.056 | 25min pv=100% + BESS discharge | |
| Otter River (A1) | 69 | 1.06 | 25min pv=100% + BESS discharge | |
| | | 0.88 | 25sh-ew+pump PV=0% BESS Charging | |
| Royalston (A1) | 69 | 1.059 | 25min pv=100% + BESS discharge | |
| | | 0.890 | 25sh-ew+pump PV=0% BESS Charging | |
| Chestnut Hill (A1) | 69 | 1.053 | 25min pv=100% + BESS discharge | |
| | | 0.89 | 25sh-ew+pump PV=0% BESS Charging | |
| Crystal Lake (B2) | 69 | 1.07 | 25sh-we pv=100% + BESS discharge | |
| | | 1.054 | 25sh-we pv=100% + BESS discharge | |

Appendix D provides the full N-0 and N-1 thermal and steady state voltage results.

5.4.4 N-1-1 Steady State Results

N-1-1 Thermal Results:

One additional thermal overload on the A-1 circuit (over and above that found for N-1 contingencies) was identified for N-1-1 contingencies. This occurs with or without [REDACTED] (QP1031) or [REDACTED] (QP1112) In-service.

Table 20 – N-1-1 Thermal Overloads (Incremental to N-1 Overloads)

| Worst case Loading at or above 100% of LTE Rating | | | | Base case | 1 st CONTINGENCY (Loss of) | 2 nd CONTINGENCY (Loss of) |
|--|----|------------|-----------------|-------------------------------------|--|--|
| Overloaded Facility | KV | LTE Rating | Loading (% LTE) | | | |
| A-1S [Pratts Jct – E Westminster] (2/0 Cu O/H line) | 69 | | | 25sh-ew+pump PV=0% BESS Charging | | |

Two additional thermal overloads (over and above that found for N-1 contingencies) were identified on the E-5/F-6 circuits with [REDACTED] (QP1031) in place.

**Table 21 – Additional N-1-1 Thermal Overloads
(w/ [REDACTED] (QP1031) In-service)**

| Worst case Loading at or above 100% of LTE Rating | | | | Base case | 1 st CONTINGENCY (Loss of) | 2 nd CONTINGENCY (Loss of) |
|---|----|---------------|--------------------|--|--|--|
| Overloaded Facility* | KV | LTE Rating | Loading (% LTE) | | | |
| E-5E [Millbury- Pondville] (477 ACSR) | 69 | | | 25ll-we-pv=100% + BESS discharge 25pk-we-pv=100% + BESS discharge | | |
| F-6E [Millbury- Pondville] (477 ACSR) | 69 | | | 25ll-we-pv=100% + BESS discharge 25pk-we-pv=100% + BESS discharge | | |

*All additional Overload facilities are due to the inclusion of QP1031 [REDACTED] only, not QP1112 [REDACTED].

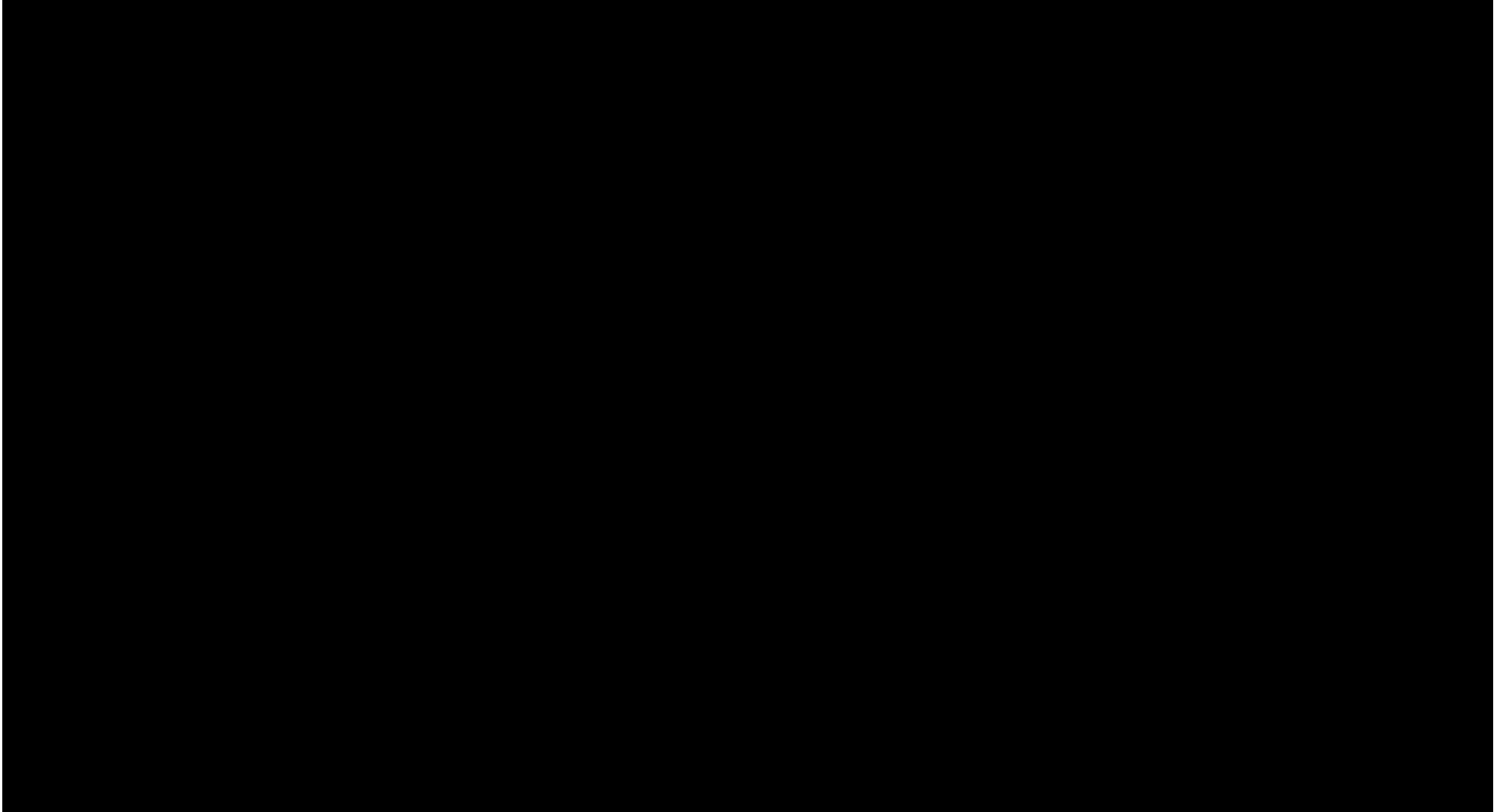
N-1-1 Voltage Results:

No additional voltage problems (over and above those found for N-1 contingencies) were identified for N-1-1 contingencies. This is true with or without [REDACTED] (QP1031) or [REDACTED] (QP1112) In-service.

Transmission Upgrades Required for Group 3 DER

- **A1/B2 line rebuild/reconductor:** The thermal overloads identified on the A1/B2 69 kV transmission lines will be eliminated by an asset condition project already scheduled for the A1/B2 lines which involves the complete rebuild of the lines using 795 ACSS conductor (ISD 2027)
- **Royalston Breaker Additions:** 69 kV breaker additions at Royalston substation are needed to eliminate voltage violations along the A1/B2 lines caused by the Group 3 DER after the A1/B2 rebuild is complete. These breaker additions are already required as part of the asset condition project to rebuild of the A1/B2 lines. Note that with the Royalston breakers in place, along with the rebuilt A1/B2 lines, the Chestnut Hill 69 kV substation will be supplied via two radial taps from A1 and B2 (unlike the existing supply to Chestnut Hill substation, which involves a loop through of the A-1 line). This new arrangement is shown in the following one-line diagram. The Chestnut Hill substation is also scheduled to be rebuilt in 2026 due to asset condition issues.
- **Vernon 69 kV substation rebuild:** 69 kV equipment at Vernon substation must be upgraded to eliminate overloads on the A-1N and B-2N 69 kV circuits. These overloads occur when both DER Group 3 is connected, and the A1/B2 are reconductored (decreases impedance). There is an asset condition project already planned to rebuild Vernon station (which will be named “Huntington” substation) in 2026, which will eliminate the overloads.
- **E5/F6 line rebuild/reconductor:** The thermal overloads on the E5/F6 69 kV transmission lines caused by the combination of [REDACTED] (QP1031) and Group 3 DER will be eliminated by the rebuild of both E5/F6 lines and reconductor with 795 ACSS conductor. The rebuild of both E5/F6 lines is already planned due to asset condition issues, and will be completed by year 2030. Note that if QP1031 is withdrawn, Group 3 DER does not cause the E5/F6 lines to become overloaded.

Figure 9 – Asset Condition Projects Planned for A1/B2 69 kV Corridor



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5.5 Group 3 DER that Can't Connect until Transmission Upgrades are Built

The following Group 3 DER can't interconnect until the A-1/B-2 69 kV transmission lines are rebuilt, the Royalston Breakers installed, and the Vernon substation is rebuilt:

| PPA ID | ISO QP Number | NGrid Case Number | Developer/Project Name | Substation |
|----------------|---------------|-------------------|------------------------|------------------|
| NEP-22-G03-036 | 1174 | 290747 | | Crystal Lake |
| NEP-22-G03-037 | 1175 | 301762 | | East Westminster |
| NEP-22-G03-041 | 1183 | 318176 | | Royalston |

If [REDACTED] (QP1031) goes in-service, the following Group 3 DER can't interconnect until the E5/F6 69 kV line rebuild is completed:

| PPA ID | ISO QP Number | NGrid Case Number | Developer/Project Name | Substation |
|----------------|---------------|-------------------|------------------------|---------------|
| NEP-22-G03-028 | 1177 | 281385 | | Lashaway |
| NEP-22-G03-029 | 1177 | 283873 | | Lashaway |
| NEP-22-G03-032 | 1179 | 178171 | | Meadow Street |
| NEP-22-G03-031 | 1179 | 178483 | | Meadow Street |
| NEP-22-G03-030 | 1179 | 193213 | | Meadow Street |
| NEP-22-G03-022 | 1188 | 178170 | | Ware |
| NEP-22-G03-023 | 1188 | 191401 | | Ware |
| NEP-22-G03-024 | 1188 | 191403 | | Ware |
| NEP-22-G03-025 | 1188 | 191405 | | Ware |

6 TRANSIENT STABILITY ANALYSIS

Stability testing was performed with all Group 1, 2 and 3 DER in-service, along with the transmission upgrades required for the interconnection of Group 3 DER, described in the previous sections. The stability testing was performed according to all applicable reliability standards. The purpose of the testing is to verify that the addition of the Group 3 DER and associated transmission upgrades do not cause significant adverse impact on the stability of the New England transmission system.

PSS/E Rev 34 was used to conduct the stability simulations.

6.1 Stability Performance Criteria

Normal Contingency (NC) Criteria

- Both system wide stability and individual unit stability must be maintained for all normal design contingencies. Individual generating units ≥ 5 MW or any set of units totaling more than 20 MW shall not lose synchronism or trip off due to voltage, frequency or other protection, except for the units that are tripped for fault clearing.
- A 53% reduction in the magnitude of system oscillations must be observed over four periods of the oscillation.

Bulk Power System (BPS) Testing

BPS testing is performed to determine the impact of the Project on facilities classified as part of the Bulk Power System (BPS), in accordance with revision 2 of the NPCC Document A-10, dated March 27, 2020, "Classification of Bulk Power System Elements". The criteria for BPS testing are as follows.

Acceptable BPS Responses

- A 53% reduction in the magnitude of system oscillations observed over four periods.
- Loss of source up to 1200 MW

Unacceptable BPS Responses

- Transiently unstable, with wide spread system collapse.
- Transiently stable, with undamped or sustained power system oscillations.
- Loss of source greater than 1200 MW.

NEPOOL Voltage SAG Guidelines

For Normal Contingencies, the minimum post-fault positive sequence voltage sag must remain above 70% of nominal voltage and must not exceed 250 milliseconds below 80% of nominal voltage within 10 seconds following a fault. These limits are supported by the typical sag tolerances shown in IEEE Standard 1346-1998.

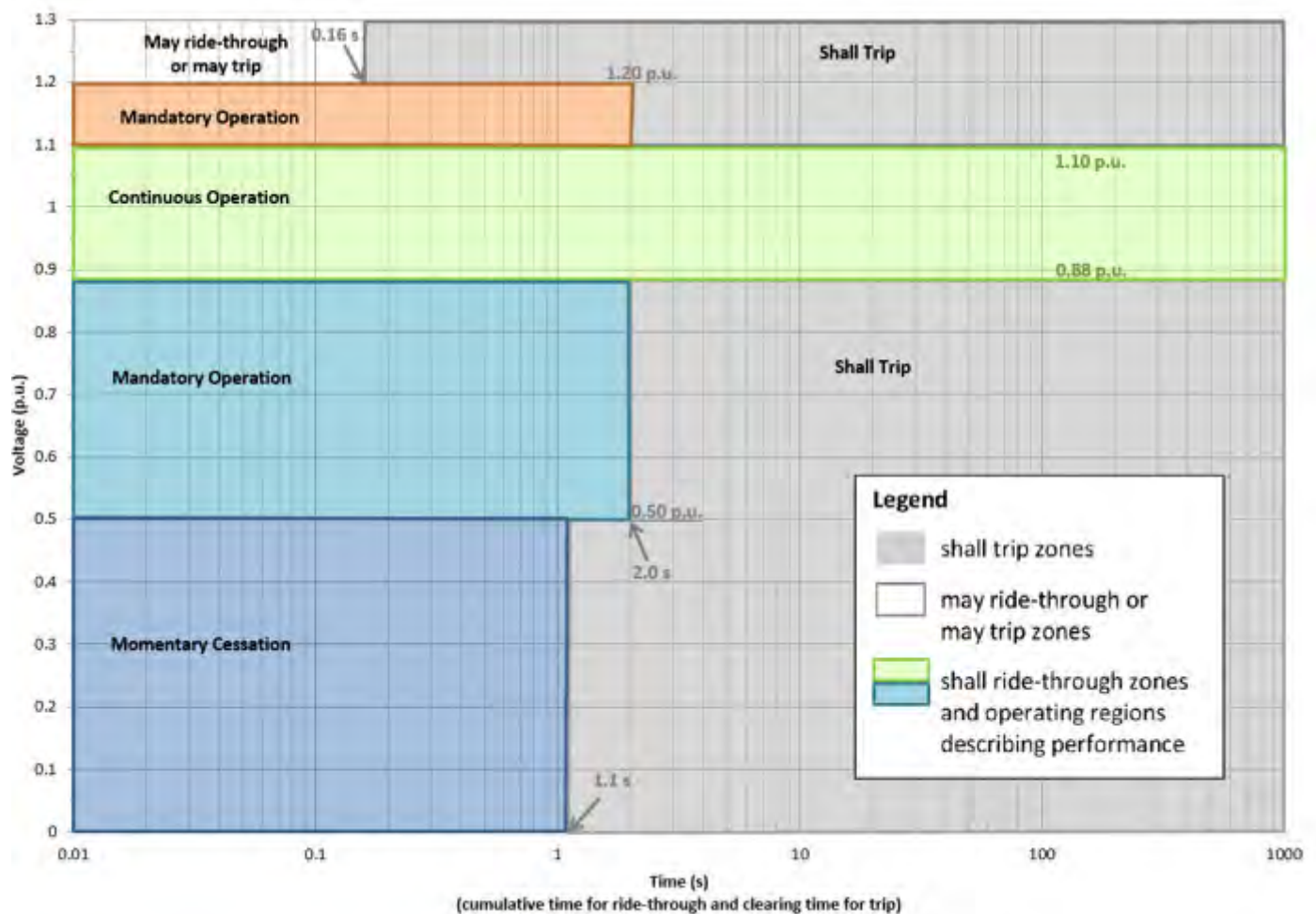
6.2 Voltage and Frequency Ride-Through Capability of DER

Groups 1, 2 and 3 DER do not have the same ride-through requirements. Groups 1 and 2 had an earlier version “Source Requirements Document” (SRD) applied to their interconnection requirements compared to the SRD applied to Group 3.

6.2.1 Voltage Ride-Through Capability for Groups 1 and 2 DER

The Voltage Ride-Through capability of Groups 1 and 2 DER were modeled according to the SRD that was applied to their interconnection, which is shown below.

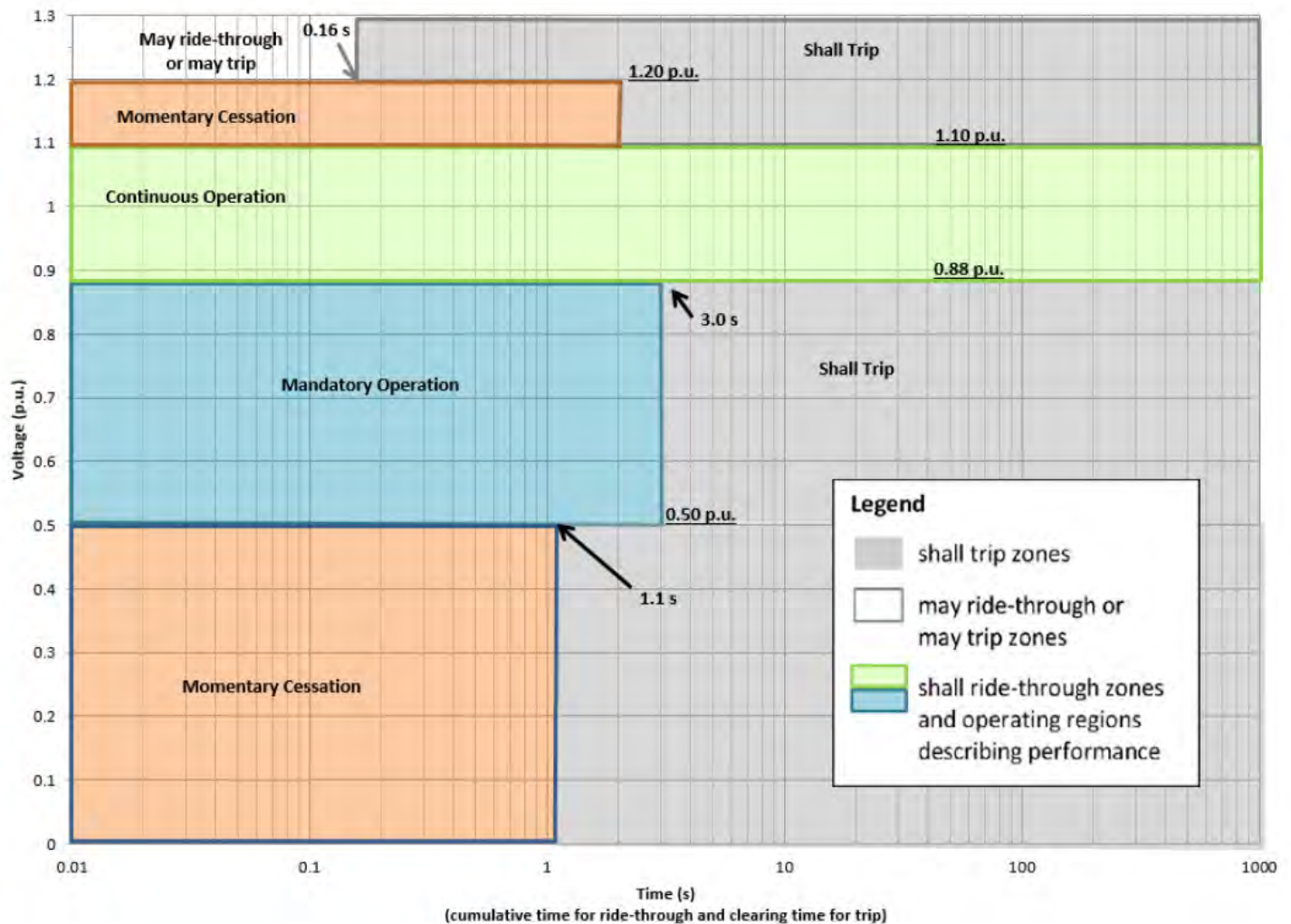
Figure 10 - Groups 1 and 2 Voltage Ride-Through Capability Curve



6.2.2 Voltage Ride-Through Capability for Group 3 DER

The Voltage Ride-Through capability of Group 3 DER is shown below. Note that the SRD was revised for Group 3 of the Western MA Cluster DER. Note that the only change pertaining to voltage ride-through in the revised SRD is that it extends the “Mandatory Operation” region from 2.0 seconds to 3.0 seconds. All Group 3 DER were modeled according to this voltage ride through curve.

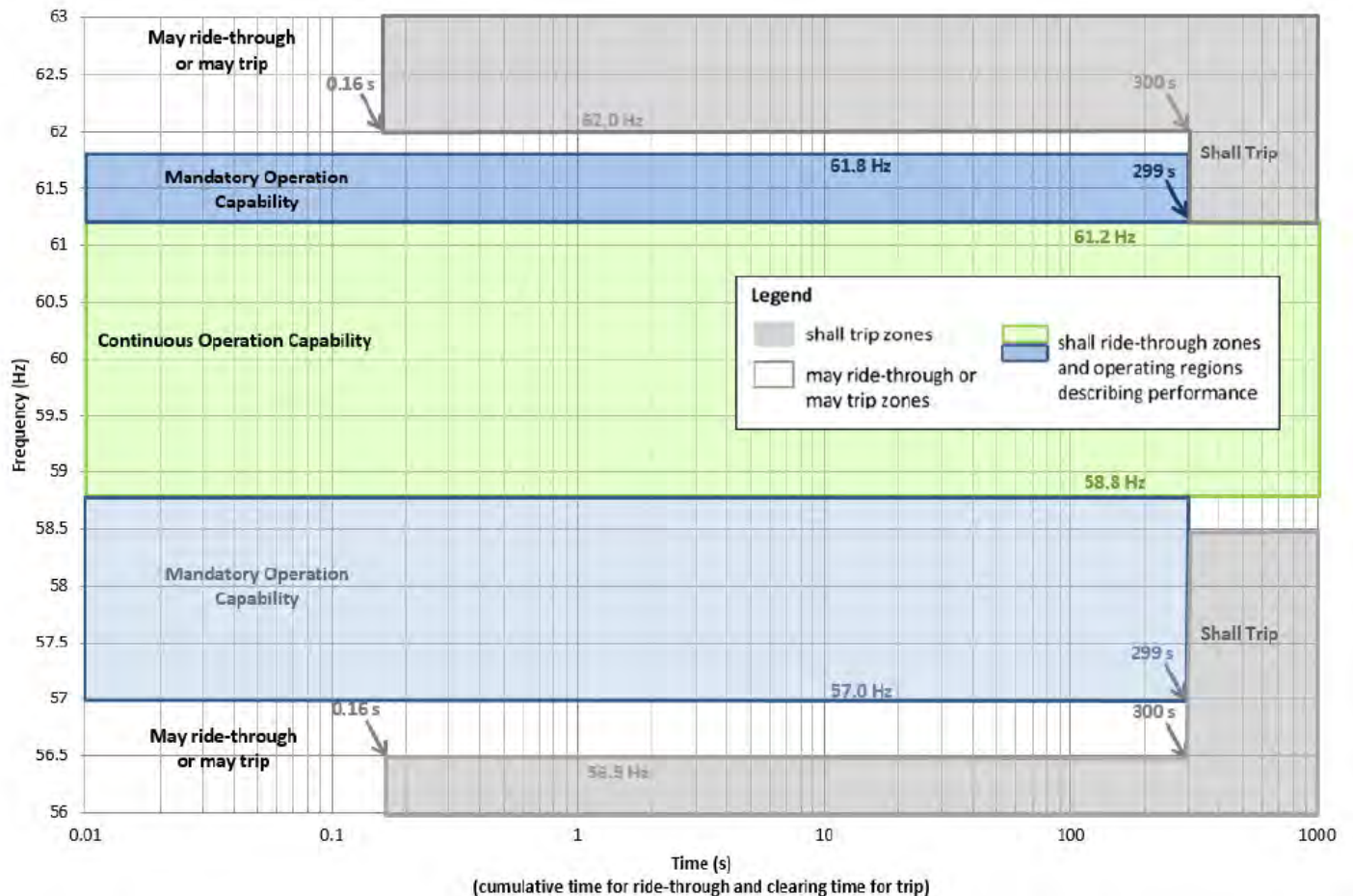
Figure 11 - Group 3 Voltage Ride-Through Capability Curve



6.2.3 Frequency Ride-Through Capability for Group 1, 2 and 3 DER

The Frequency Ride-Through requirement in the revised SRD for Group 3 is the same as in the SRD applied to Group 1 and 2. This frequency ride-through requirement curve is shown below. It was applied to all DER in Group 1, 2, and 3.

Figure 12 – Groups 1, 2, and 3 Frequency Ride-Through Curve



6.3 Frequency Response Requirement for Group 3 DER

The revised SRD for Group 3 requires that this DER respond to frequency deviations via a droop characteristic. No such requirement applies to Groups 1 and 2. Group 3 DER therefore was modeled with frequency response enabled in the stability simulations. Below are the Frequency-Droop control settings specified in the revised SRD for Group 3 DER.

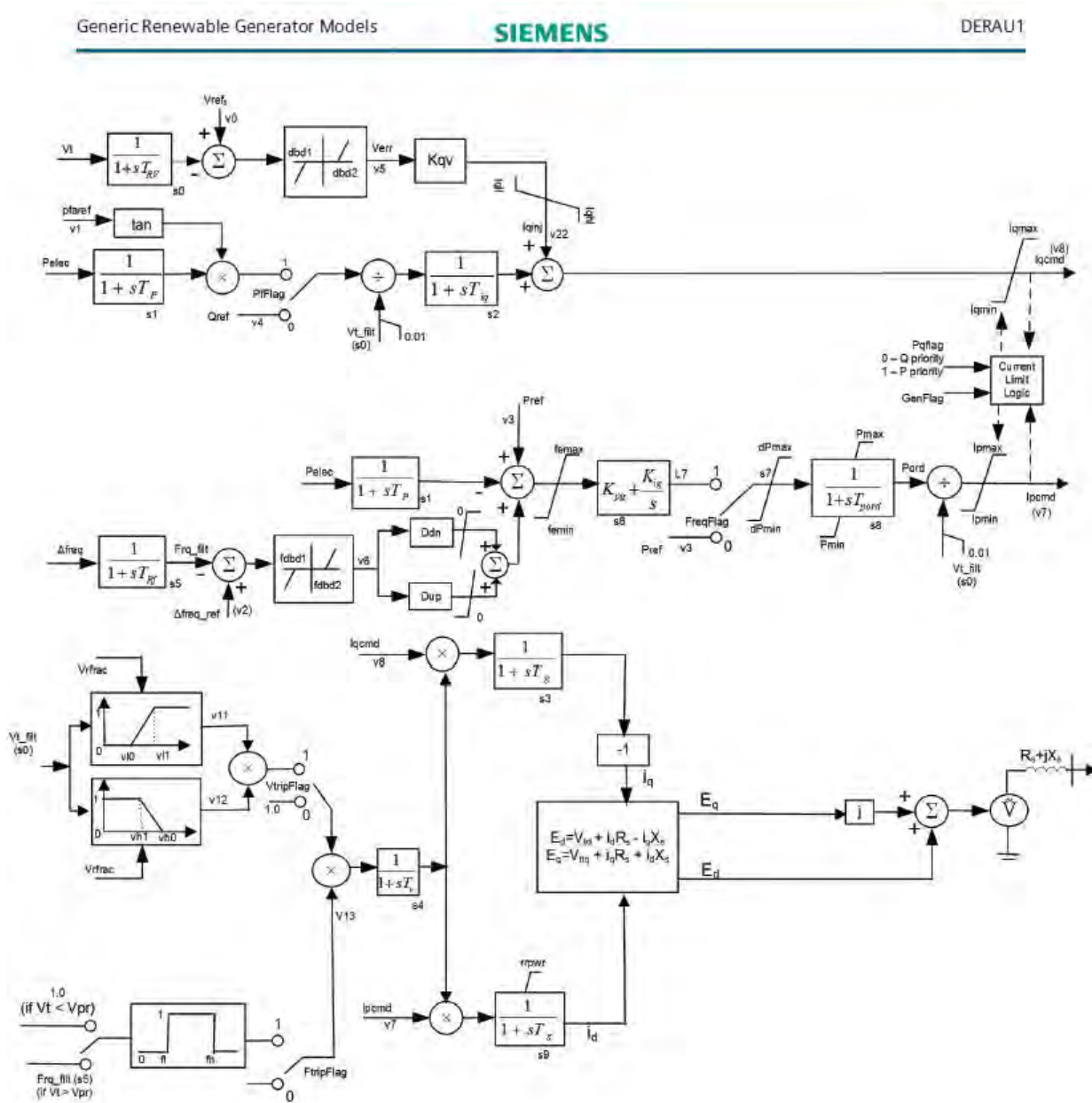
Frequency-Droop Control Settings required for Group 3 DER

| Parameter | Inverter |
|-------------------------------|----------|
| dbOF, dbUF (Hz) | 0.036 |
| kOF, kUF (Droop) | 0.05 |
| T-response (small-signal) (s) | 5 |

6.4 Stability Models for Group 1, 2, and 3 DER Between 1MW and 5MW

For Group 1, 2 and 3 DER greater than 1 MW, and less than 5 MW, this generation was modeled with the DER_A model. The block diagram of the DER_A model is shown in the following figure.

Figure 13 - DER_A Model Block Diagram



The input data that was used for the DER_A model is shown below. The parameters related to inverter dynamics characteristics are selected based on the latest guideline document from NERC.⁸ The parameters related to voltage and frequency trip settings are selected such that the inverter complies with the voltage and frequency ride-through requirement of National Grid SRD.

Table 22 - DER_A Model Parameters Assumed for Study

| Parameters | Value | | Notes |
|------------|-------------------|-------------|--|
| | Group 1 and 2 DER | Group 3 DER | |
| trv | 0.02 | 0.02 | Voltage Transducer Time constant (default) |
| trfs | 0.02 | 0.02 | Frequency measurement transducer time constant (not in NERC guidance document, but assumed 0.02, same as Voltage Transducer Time constant) |
| dbd1 | -99 | -99 | No voltage control will be modeled (default) |
| dbd2 | 99 | 99 | No voltage control will be modeled (default) |
| kqv | 0 | 0 | No voltage control will be modeled (default) |
| vref0 | 0 | 0 | No voltage control will be modeled (default) |
| tp | 0.02 | 0.02 | Power Transducer Time constant (default) |
| tiq | 0.02 | 0.02 | Q control Transducer Time constant (default) |
| ddn | 0 | 20 | reciprocal of droop for over-frequency conditions |
| dup | 0 | 0 or 20 | reciprocal of droop for under-frequency conditions (0 for solar and wind units. 20 for storage device) |
| fdbd1 | -99 | -0.0006 | deadband (default) |
| fdbd2 | 99 | 0.0006 | deadband (default) |
| femax | 0 | 99 | Freq error up limit (default) |
| femin | 0 | -99 | Freq error low limit (default) |
| pmax | 1 | 1 | 1 for wind, solar and battery units |
| pmin | 0 or -1 | 0 or -1 | 0 for wind, solar units. -1 for battery units |
| dpmax | 99 | 99 | Power reference max ramp rate (default) |
| dpmin | -99 | -99 | Power reference min ramp rate (default) |
| tpord | 0.02 | 5 | Power Filter Open loop time constant (default) |
| kpg | 0 | 0.1 | Not mappable to interconnection standards (0, for no frequency control) |
| kig | 0 | 10 | Not mappable to interconnection standards (0, for no frequency control) |
| imax | 1.2 | 1.2 | Maximum converter current (typical inverter max output) |
| vl0 | 0.50 | 0.50 | Voltage at head of feeder at which DER at head of feeder starts tripping. |
| vl1 | 0.55 | 0.55 | Voltage at head of feeder at which DER at tail of feeder trips. Assume 5% voltage drop across Feeder. Amount of DER dropped will follow a linearly increasing amount until vl0, when all will be dropped |
| vh0 | 1.15 | 1.15 | Voltage at head of feeder at which DER at tail of feeder trips. Assume 5% voltage drop across feeder |
| vh1 | 1.1 | 1.1 | Voltage at head of feeder at which DER at head of feeder starts tripping. Amount of DER dropped will follow a linearly increasing amount until vh0, when all will be dropped |

⁸ https://www.nerc.com/comm/PC_Reliability_Guidelines_DL/Reliability_Guideline_DER_A_Parameterization.pdf

| Parameters | Value | | Notes |
|------------|-------------------|-------------|---|
| | Group 1 and 2 DER | Group 3 DER | |
| tvlo | 1.1 | 1.1 | low voltage cut-out timer corresponding to voltage vlo |
| tvll | 1.1 | 1.1 | low voltage cut-out timer corresponding to voltage vll |
| tvh0 | 2.0 | 2.0 | High voltage cut-out timer corresponding to voltage vho |
| tvhl | 2.0 | 2.0 | High voltage cut-out timer corresponding to voltage vhl |
| vrfrac | 1 | 1 | Per unit of DER that comes back after tripping (1 = 100% of DER comes back online if terminal voltage recovers above vlo (0.5 pu) within 1.1 seconds; 0 = 100% of DER is tripped permanently if terminal voltage does not recover above vlo (0.5 pu) within 1.1 seconds). The same logic holds true for voltages that exceed vhl. |
| fltrp | 57.0 | 57.0 | Frequency trip settings per National Grid SRD |
| fhtpr | 62.0 | 62.0 | |
| tfl | 0.16 | 0.16 | |
| tfh | 0.16 | 0.16 | |
| tg | 0.02 | 0.02 | † current control time constant (inner control loops) (default) |
| rrpwr | 2.0 | 2.0 | Ramp rate for real power increase following a fault (pu/S) as per 1547-2018 to achieve 80% recovery in 0.4 sec |
| tv | 0.02 | 0.02 | time constant on the output of the multiplier (time delay for partial tripping) (default value) |
| vpr | 0.7 | 0.7 | Low voltage inhibit on frequency tripping (due to spurious spikes that occur in positive sequence stability models) - NOTE: all frequency tripping during simulations should be double checked for tripping due to spurious frequency spikes |
| iqhl | 0 | 0 | No voltage control |
| iqll | 0 | 0 | No voltage control |
| pf flag | 1 | 1 | Constant power factor (based on initial value from steady state model) |
| frq flag | 0 | 1 | Freq control (1 to enable, 0 to disable) |
| pq flag | 1 | 1 | Active current (P) priority (during large disturbances) |
| Genflag | 1 or 0 | 1 or 0 | 1 for Generator (0 is for storage device) |
| vtripflag | 1 | 1 | Enables voltage trip logic |
| ftripflag | 1 | 1 | Enables frequency trip logic |

Note that all Group 3 DER will respond to frequency deviations, while all Group 1 and 2 DER will not, due to differences in the SRD between the groups.

All DER greater than 1 MW, but less than 5 MW, is modeled aggregately as a single equivalent generator, at the distribution bus of each substation to which it is connected. The MW size of the single equivalent generator, at a specific substation, is equal to the total amount of DER (greater than 1 MW but less than 5 MW) to be connected to that substation. No distribution feeder impedance is modeled between the equivalent generator and the distribution bus to which it is connected.

6.5 Stability Models of Group 1 and 2 DER Equal to 5MW and Greater

The Group 1 and 2 DER, equal to, or greater than 5 MW, were modeled with the same PSS/E library models as used for the Group 2 study.

These generators were modeled as individual generators combined with their equivalent collection system and GSU at the low side of the substation to which they will be connected through.

These generators were modeled with a standard PSS/E library model set consisting of the following modules:

REGCA – Renewable Energy Generator/Converter Model

REECA – Renewable Energy Electrical Model

REPCA – Plant Controller model

The following projects below exceeded 5 MW for Group 2.

Table 23 - Group 2 DER Greater than 5MW

| Substation | Size (MW) |
|------------|-----------|
| Shutesbury | 10.0 |

The following projects below exceeded 5 MW for Group 1.

Table 24 - Group 1 DER Greater than 5MW

| Substation | Size (MW) |
|---------------|-----------|
| Belchertown | 8 |
| Lashaway | 6 |
| Snow Street | 12 |
| Wendell Depot | 5 |

6.6 Stability Models for Group 3 DER Equal to 5MW and Greater

The Group 3 DER, equal to, or greater than 5 MW, were modeled with the following library models for inverter based resources available in PSS/E Rev34.

- 1.) Renewable Energy Generator/Converter Model: REGC_B
- 2.) Renewable Energy Electrical Model: REEC_D
- 3.) Plant Controller model: REPCA

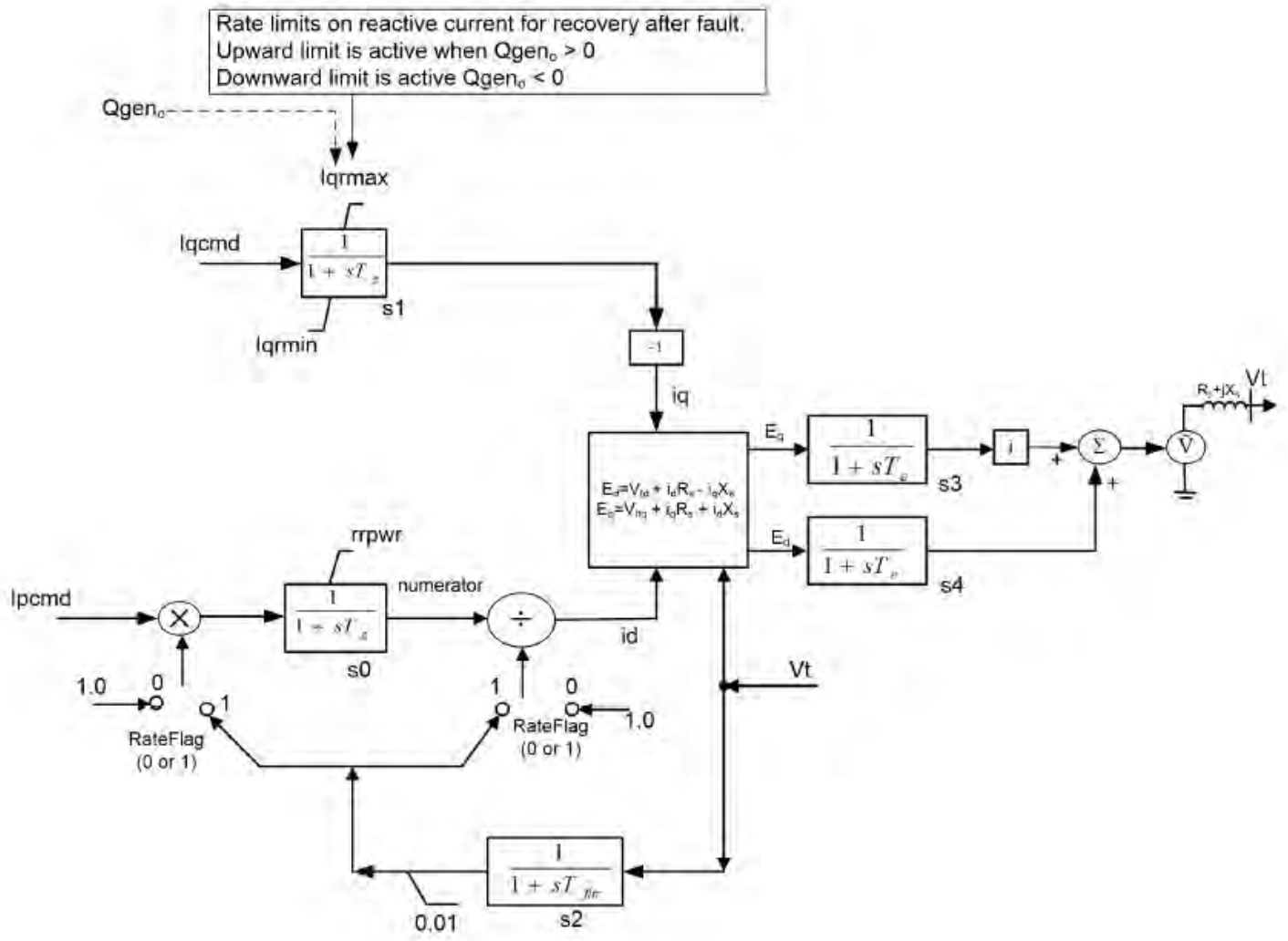
The following projects below exceeded 5 MW for Group 3.

Table 25 - Group 3 DER Greater than 5MW

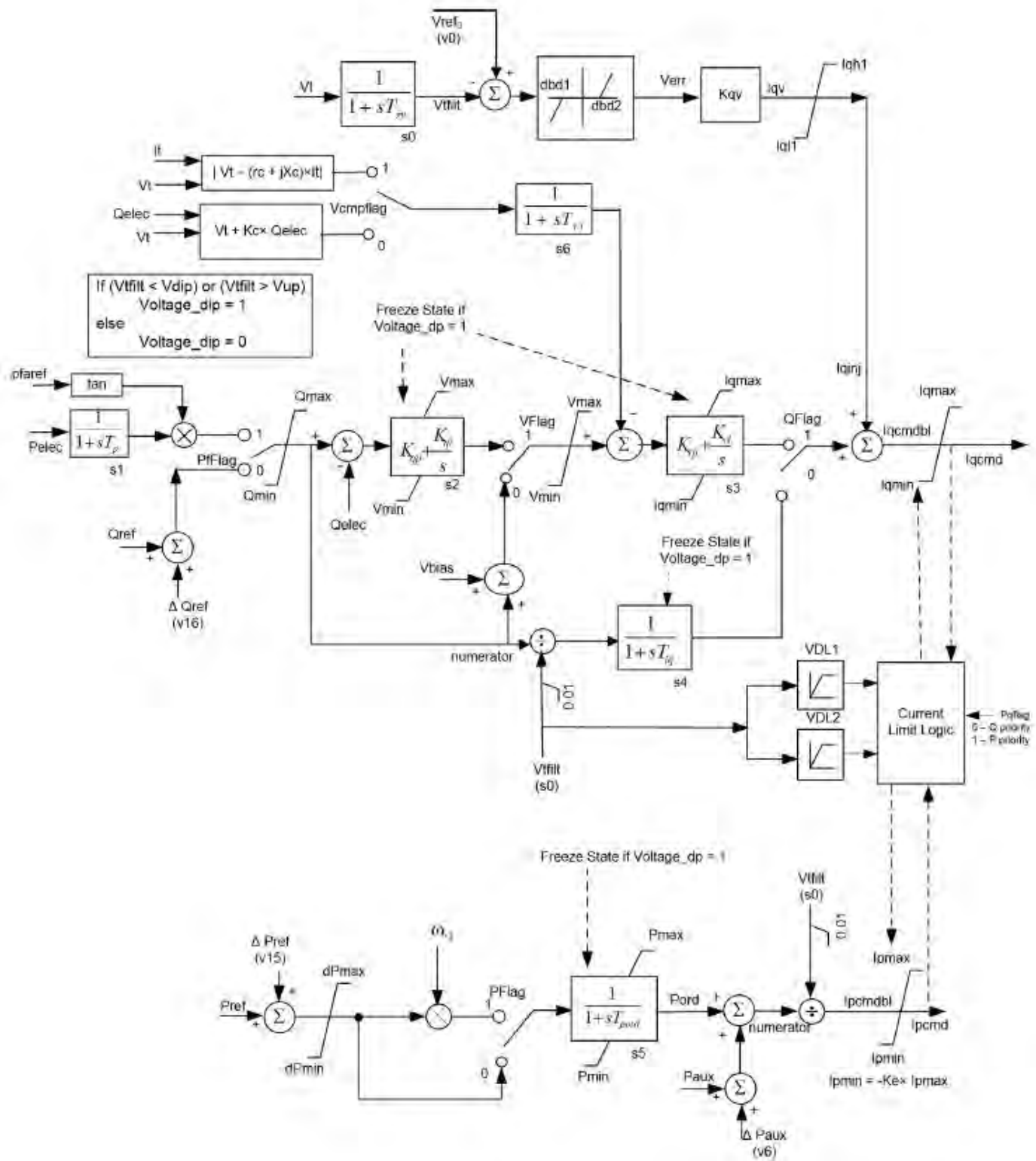
| PPA ID | Substation | Type | Size (MW) | |
|----------------|-----------------|------------|-------------------|----------------|
| | | | Discharging Limit | Charging Limit |
| NEP-22-G03-034 | Barre | BESS only | 8 | 8 |
| NEP-22-G03-036 | Crystal Lake | BESS only | 8 | 5.2 |
| NEP-22-G03-038 | East Winchendon | BESS only | 9.4 | 4.6 |
| NEP-22-G03-039 | East Winchendon | BESS only | 5.5 | 4.2 |
| NEP-22-G03-029 | Lashaway | BESS only | 10 | 7 |
| NEP-22-G03-008 | Laurel Circle | BESS only | 8 | 4.4 |
| NEP-22-G03-009 | Millbury | BESS only | 10 | 3.5 |
| NEP-22-G03-011 | North Oxford | BESS only | 8 | 6.4 |
| NEP-22-G03-013 | North Oxford | BESS only | 5.6 | 4.8 |
| NEP-22-G03-006 | Pratts Junction | BESS only | 6 | 4.5 |
| NEP-22-G03-041 | Royalston | AC Coupled | 5 | 0 |
| NEP-22-G03-015 | Snow St | BESS only | 5 | 2.5 |
| NEP-22-G03-016 | Snow St | BESS only | 5 | 2.5 |
| NEP-22-G03-017 | Snow St | BESS only | 5.5 | 6.5 |
| NEP-22-G03-001 | Stafford St | DC Coupled | 5 | 5 |
| NEP-22-G03-033 | Treasure Valley | BESS only | 10 | 5 |
| NEP-22-G03-020 | West Charlton | BESS only | 5 | 4.5 |
| NEP-22-G03-021 | West Charlton | BESS only | 10 | 4 |
| NEP-22-G03-044 | Wendell Depot | BESS only | 8 | 7.2 |
| NEP-22-G03-043 | Wendell Depot | BESS only | 10 | 8 |

The block diagrams for these models are shown in the following figures.

REGC_B Block Diagram [Source: PSS/E]

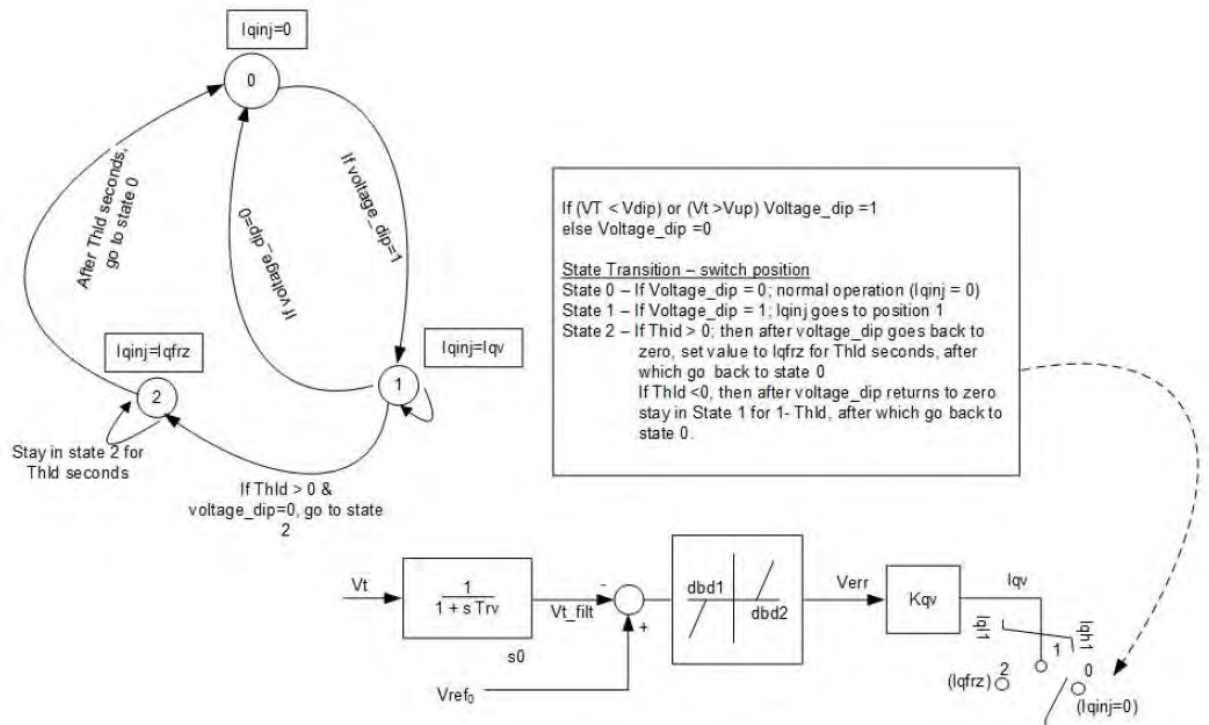


REEC_D Block Diagram [Source: PSS/E]

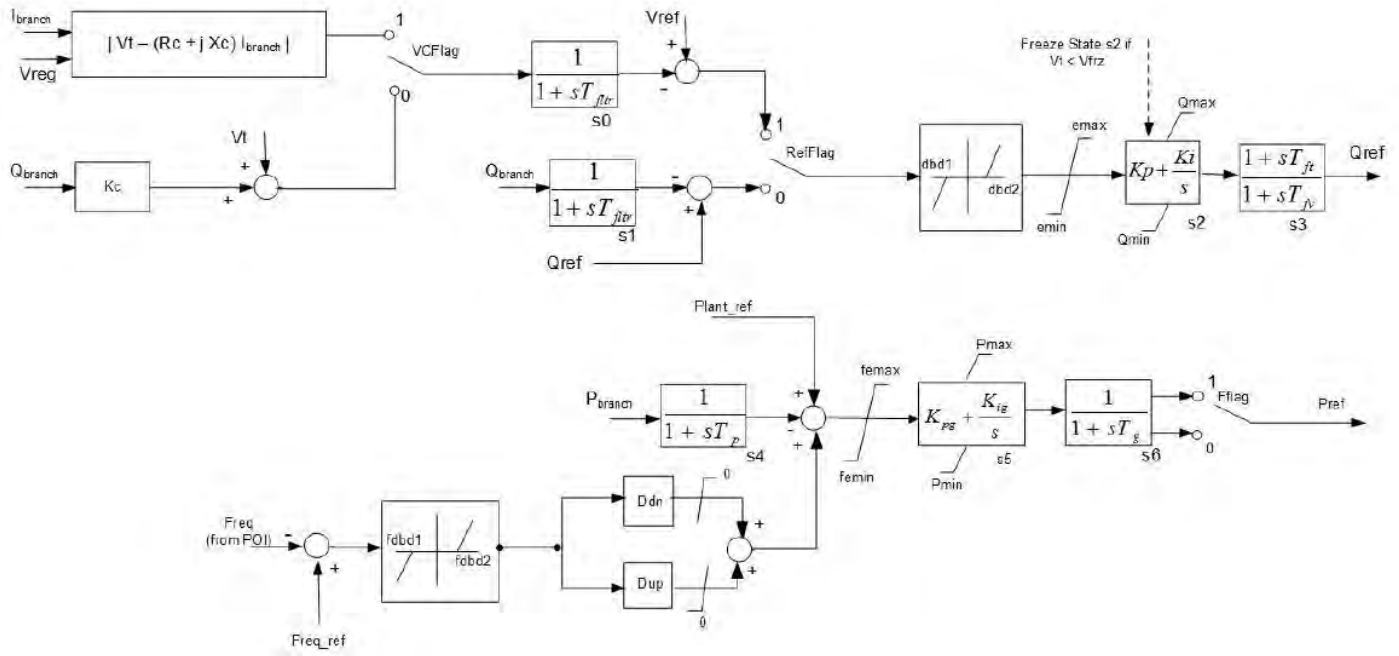


REEC_D Block Diagram – Continued:

REEC_D Block Diagram continued:
 State Transition Diagram for dynamic voltage support during high or low voltage conditions



REPC_A Block Diagram [Source: PSS/E]



6.7 Stability Analysis Case Development

In order to investigate the impact of the proposed Group 3 DER on the New England transmission system, two base cases representing the 2026 summer peak load levels and two base cases representing the 2026 light load levels, were developed for this study.

Four base cases derived from the 2026 light load levels were also developed to determine if any existing substations, that are not part of the NPCC Bulk Power System (BPS) become part of the BPS as a result of the addition of Group 3 DER.

Year 2026 ISO-NE dynamics cases (PSS/E Rev 34), released in April 2021, were used for this transient stability assessment.

6.8 Stability Case Summaries

The following table summarizes the interface levels and generation dispatches for the stability base cases that includes Group 1,2 and 3 DER.

Table 26 - Stability Case Summaries for Design Contingency Testing

| Interface Name | Interface Flows (MW) | | | |
|--------------------------------|----------------------|---------|------------------|---------|
| | Peak Load Case | | Light Load Cases | |
| | 23pk-ew | 23pk-we | 23ll-ew | 23ll-we |
| NB-NE | 808 | 1017 | 1013 | 1013 |
| ORR_SOUTH | 1375 | 1189 | 1326 | 1326 |
| SURW_SOUTH | 1359 | 1183 | 1611 | 1667 |
| ME-NH | 1996 | 1203 | 1978 | 2035 |
| EAST-WEST | 3104 | -3072 | 3917 | -2527 |
| NE-NY | 1290 | -1467 | 1223 | -1303 |
| NNE-SCOB+394 | 3658 | 2961 | 3021 | 1697 |
| NORTH-SOUTH | 3724 | 2826 | 4060 | 1682 |
| SEMA/RI – NE | 2746 | -2559 | 1121 | -1255 |
| HIGHGATE_IMP | 224 | 224 | 224 | 224 |
| SDNDPD_IMP | 2000 | 2000 | 2000 | 0 |
| CT IMPORT | 3412 | 309 | 563 | -144 |
| Cross sound cable Export to NY | 101 | 101 | 101 | 101 |
| | | | | |
| Bear Swamp | 666 | 666 | -666 | 0 |
| Northfield | 1180 | 1180 | -1000 | 0 |
| Altresco | 197 | 197 | 197 | 197 |
| Millennium | 412 | 412 | OOS | 285 |

Table 27 - Stability Light Load Case Summaries for BPS Simulations

| Interface Name | Interface Flows (MW) | | | |
|--------------------------------|----------------------|-------|-------|-------|
| | WMAVT | BOS | ME_C | SEMA |
| NB-NE | 1013 | 1013 | 1013 | 1013 |
| SURW_SOUTH | 1663 | 896 | 1252 | 897 |
| ME-NH | 1437 | 1255 | 1609 | 1256 |
| EAST-WEST | -1578 | 3790 | 3867 | 4179 |
| NE-NY | 1054 | 1210 | 1279 | 1429 |
| NNE-SCOB+394 | 3176 | 2678 | 3089 | 2447 |
| NORTH-SOUTH | 2980 | 2559 | 3237 | 2066 |
| SEMA/RI - NE | -1816 | 2367 | 1743 | 3174 |
| HIGHGATE_IMP | 224 | 224 | 224 | 224 |
| SNDYPD_IMP | 0 | 2000 | 2000 | 2000 |
| CT IMPORT | 401 | 1100 | 1100 | 1148 |
| Cross sound cable Export to NY | 101 | 101 | 101 | 101 |
| Bear Swamp | 666 | -666 | -666 | -666 |
| Northfield | 1180 | -1100 | -1100 | -1100 |
| Alresco | 197 | 197 | 197 | 197 |
| Millenium | 412 | 0 | 0 | 0 |

6.9 Stability Study Matrix

To test the impact of the DER, Group 1,2 and 3 DER were added to each case, according to the following table, and dispatched against generation in Connecticut. Dispatching the DER against Connecticut will maintain the same East-West, and NY-NE transfer levels, compared to the pre-DER base cases.

Table 28 – Study Matrix for Stability Analysis

| Load Level | Bias | Group 3 DER | | Group 1 and 2 DER | Pre Group 1 and 2 DER | FERC BESS projects under Study | Comments |
|------------------|-------|------------------|-----------|-------------------|---|---|---|
| | | BESS output | PV output | PV output | PV output | | |
| Summer Peak load | E-W | 100% Charging | 26% | 26% | only ≥5MW projects in WMA already modeled in the basecases were turned on | ██████████ (QP1031) and ██████████ (QP1112) were modeled in the study | All 1-5MW projects were modeled using DER_A model using parameters based on the latest guideline document from NERC. All ≥ 5 MW projects were modeled using standard renewable energy models parametrized by individual project developers |
| | W-E | 100% discharging | 100% | 100% | | | |
| Light Load | E-W | 100% charging | 26% | 26% | | | |
| | W-E | 100% discharging | 100% | 100% | | | |
| BPS | WMAVT | 100% discharging | 100% | 100% | | | |
| | BOS | | | | | | |
| | ME-C | | | | | | |
| | SEMA | | | | | | |

6.10 BPS Contingencies

The following simulations were conducted to determine if any existing substations become classified as Bulk Power System (BPS) substations as a result of the addition of Group 3 DER. Further, whether any of the new stations, required to accommodate the interconnection of the Group 3 DER, need to meet BPS design requirements.

Table 29 - Bulk Power System (BPS) Contingencies

| Contingency Name | Type | kV | Location | Clearing Times (cycles) | Protection Groups | Light Load Results | | | |
|------------------|------|-----|------------|-------------------------|-------------------|--------------------|------|------|-------|
| | | | | | | BOS | ME_C | SEMA | WMAVT |
| BS-230-BPS | BPS | 230 | Bear Swamp | | | | | | |
| BS-115-BPS | BPS | 115 | Bear Swamp | | | | | | |
| PJ-115-BPS | BPS | 115 | Pratts Jct | | | | | | |

| Contingency Name | Type | kV | Location | Clearing Times (cycles) | Protection Groups | Light Load Results | | | |
|------------------|------|-----|-------------------|-------------------------|-------------------|--------------------|------|------|-------|
| | | | | | | BOS | ME_C | SEMA | WMAVT |
| PJ-230-BPS | BPS | 230 | Pratts Jct | | | | | | |
| Palmer-115-BPS | BPS | 115 | Palmer | | | | | | |
| Carp-115-BPS | BPS | 115 | Carpenter Hill | | | | | | |
| Flagg-115-BPS | BPS | 115 | Flagg Pd | | | | | | |
| Stafford-115-BPS | BPS | 115 | Stafford St (new) | | | | | | |

6.11 N-1 Stability Contingencies

Several Breaker Failure (BF) contingencies were tested. These Breaker Failures were first tested with a 3-phase initiating fault, which is categorized as an Extreme Contingency. If this test failed the performance requirements outlined in ISO-NE PP-3, a corresponding design contingency is tested (Breaker failure with single line to ground imitating fault); otherwise, no corresponding design contingency is tested.

Table 30 - N-1 Breaker Failure Contingencies

| Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|-----|-----------------------|-------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| BS-1205E-BF | EC | 230 | | | | | | | |
| BS-T97-BF | EC | 115 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|-----|-----------------------|-------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| ML-0802-BF | EC | 345 | | | | | | | |
| WM-105-BF | EC | 345 | | | | | | | |
| SP-3521-BF | EC | 345 | | | | | | | |
| CH-321-BF | EC | 345 | | | | | | | |
| CH-174W-BF | EC | 115 | | | | | | | |
| CH-175-BF | EC | 115 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|-----|-----------------------|-------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| PJ-69kV-TIE-BF | EC | 69' | | | | | | | |
| NFLD-2T-BF | EC | 345 | | | | | | | |
| PALM-X176-BF | EC | 115 | | | | | | | |
| AD-3T5T-BF | EC | 115 | | | | | | | |
| STAFF-2728E-BF | EC | 115 | | | | | | | |
| STAFF-B128E-BF | EC | 115 | | | | | | | |
| STAFF-2728W-BF | EC | 115 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|----|-----------------------|-------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| | | | | | | | | | |

Several design contingencies were tested on the transmission system facilities located along the Western and Central Massachusetts transmission corridor.

Table 31 - N-1 Stability Design Contingencies

| Contingency Name | Type | kV | Location/ Description | Clearing times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|-----|--------------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| V174-CH | NC | 115 | | | | | | | |
| V174-ML | NC | 115 | | | | | | | |
| E205E-PJ | NC | 230 | | | | | | | |
| E205W-BS | NC | 230 | | | | | | | |
| 354-NFId | NC | 345 | | | | | | | |
| 354-Ludlow | NC | 345 | | | | | | | |
| S197-BS | NC | 115 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|-------------------------------|------|-----|--------------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| E131-BS | NC | 115 | | | | | | | |
| Z126-WEB | NC | 115 | | | | | | | |
| E5-WARE | NC | 69 | | | | | | | |
| E5-F6E-DCT- Millbury | NC | 69 | | | | | | | |
| A1S-B2S- DCT-Gardner | NC | 69 | | | | | | | |
| A1N-B2N- DCT- Royalston | NC | 69 | | | | | | | |
| D4-Vernon | NC | 69 | | | | | | | |
| J136N-BELFS | NC | 115 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|-----|--------------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| O15N- PALM | NC | 69 | | | | | | | |
| A127-ERV | NC | 115 | | | | | | | |
| A127-ST | NC | 115 | | | | | | | |
| I135-FP | NC | 115 | | | | | | | |
| I135-CHINK | NC | 115 | | | | | | | |
| X176E-PALM | NC | 115 | | | | | | | |
| X176-LUD | NC | 115 | | | | | | | |
| W175W-PALM | NC | 115 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|----------------------------|------|-----|--------------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| SP-HVDC Bipole | NC | 450 | | | | | | | |
| STAFF- 2728E-BF- SLG | NC | 115 | | | | | | | |
| STAFF- B128E-BF- SLG | NC | 115 | | | | | | | |
| STAFF- 2728W-BF- SLG | NC | 115 | | | | | | | |
| PJ-69kV-TIE- BF-SLG | NC | 69' | | | | | | | |
| BS-1205E-BF- SLG | NC | 230 | | | | | | | |
| BS-1205W- BF-SLG | NC | 230 | | | | | | | |

| Contingency Name | Type | kV | Location/ Description | Clearing times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|------------------|------|-----|--------------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| | | | | | | EW | WE | EW | WE |
| BS-T97-BF-SLG | NC | 115 | | | | | | | |
| BS-T31-BF-SLG | NC | 115 | | | | | | | |
| AD-3T5T-BF-SLG | NC | 115 | | | | | | | |

6.12 N-1-1 Stability Contingencies

Several design contingencies were tested with an initial element out of service as shown in the table below. Any generation backdown that is required between contingencies were found not to exceed existing limits.

Table 32 - N-1-1 Stability Design Contingencies

| Initial N-1 | Post N-1 | N-1-1 Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|--|--------------------|------------------------|------|-----|-----------------------|-------------------------|-------------------|--------------------|----|-------------------|----|
| Line Out | System Adjustments | | | | | | | EW | WE | EW | WE |
| 301/302 345 kV [Ludlow-Millbury] | None | E205E-PJ | NC | 230 | | | | | | | |
| | | Z126-WEB | NC | 115 | | | | | | | |
| | | S197-BS | NC | 115 | | | | | | | |
| | | V174-ML | NC | 115 | | | | | | | |
| | | NFLD-2T-BF-SLG | NC | 345 | | | | | | | |

| Initial N-1 | Post N-1 | N-1-1 Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|-------------|-----------------------|------------------------------|------|-----|-----------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| Line Out | System Adjustments | | | | | | | EW | WE | EW | WE |
| | | | | | | | | | | | |
| | | NFLD-9T- BF-SLG | NC | 345 | | | | | | | |
| | | Ludlow-5T- BF-SLG | NC | 345 | | | | | | | |
| | | CH-174W- BF-SLG | NC | 115 | | | | | | | |
| | | 381-NFLD | NC | 345 | | | | | | | |
| | | FITZ-3791- BF-SLG | NC | 345 | | | | | | | |
| | | SP-HVDC Bipole | NC | 450 | | | | | | | |

| Initial N-1 | Post N-1 | N-1-1 Contingency Name | Type | kV | Location/ Description | Clearing Times (cycles) | Protection Groups | Light Load Results | | Peak Load Results | |
|---|-----------------------|------------------------------|------|-----|-----------------------|----------------------------|-------------------|--------------------|----|-------------------|----|
| Line Out | System Adjustments | | | | | | | EW | WE | EW | WE |
| | | BS-T97-BF-SLG | NC | 115 | | | | | | | |
| Northfield 345-115 kV auto | none | A127-ST | NC | 115 | | | | | | | |
| Fitzwilliam 345-115 kV auto | none | I135-FP | NC | 115 | | | | | | | |
| S-197 115 kV line [Bear Swamp- Deerfield] | None | B2S-PJ | NC | 69 | | | | | | | |
| A-1S from Pratts to Otter River | None | B2S-CL | NC | 69 | | | | | | | |
| E-5E from Millbury – Meadow St | None | O15N-Ware | NC | 69 | | | | | | | |

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7 SHORT CIRCUIT ANALYSIS

ASPEN Version 14 was used to conduct the short circuit simulations for this study.

7.1 Short Circuit Models

ISO-NE's N+5 (five year out) short circuit case, dated January 1st, 2020 was used for this study. Group 1 and 2 DER were already included in this case. The Group 3 DER was modeled at each substation, in an aggregate fashion, with a single equivalent generator at the low side of each substation to which the DER will be connected. The MW size of the single equivalent generator, equaled the total amount of DER (greater than 1 MW) to be connected to that substation.

7.2 Methodology and Criteria

The modeling assumptions and short circuit performance criteria, including settings used in Aspen's breaker rating module, are per National Grid's TGP34 'Circuit Breaker Fault Current Assessment Guide' and its associated TGP34 Technical Guidelines.

The aggregate MWs for Group 3 DER was combined with the aggregate MWs for Group 1 and 2 DER, to come up with a single aggregate generator at each substation, as applicable.

Voltage Controlled Current Source (VCCS) models were used for all PV inverters in Groups 3, as were for Groups 1 and 2. The VCCS models were assumed to deliver up to 1.2 p.u. of its nameplate current during fault conditions. Distinct Power Factor (PF) angles were modeled for several different voltage levels for each inverter. The PF Angle (degrees) for each DER terminal voltage was calculated based on recommendations provided in the ASPEN "Technical Bulletin on Modeling Type-4 Wind Plants and Solar Plants". The following figure is an example of an ASPEN model that was used for a 9 MW aggregate unit.

Figure 14 - Sample VCCS model

Voltage Controlled Current Source

At bus BEAR SW 13-5 13.8 kV

| Voltage (pu)* | Current (A) | PF Angle (deg) |
|---------------|-------------|----------------|
| 1.0 | 377. | 0. |
| 0.9 | 452. | -11.3 |
| 0.8 | 452. | -31. |
| 0.7 | 452. | -56.4 |
| 0.6 | 452. | -56.4 |
| 0.5 | 452. | -56.4 |
| 0.4 | 452. | -56.4 |
| 0.3 | 452. | -56.4 |
| 0.1 | 452. | 90. |

MVA rating = 9. FLC

*Pos. seq. voltage measured at

☒ Device terminal

☐ Network side of transformer

Limits on voltages at terminal

Max = 1.2 times prefault value

Min = 0. pu

☐ Shut down based on min phase voltage

Sort Grid

Memo

Date In-service: [N/A](#) Out-of-service: [N/A](#)

Tags: [None](#)

OK Cancel Help

[Last changed Mar 02, 2020](#)

The figure below shows the ASPEN solution options assumed for the short circuit analysis. Note that current limits were not enforced for inverter-based generation modeled with current limited synchronous generators. This is a slightly conservative assumption, but not overly conservative since there is very little, if any inverter-based generators modeled with current limited synchronous generators in the study area.

Figure 15 - ASPEN Solution Options Assumed for short circuit analysis

ANSI/IEEE Breaker Checking Options

| | |
|--|---|
| Fault Types <input checked="" type="checkbox"/> 3LG <input checked="" type="checkbox"/> 2LG <input checked="" type="checkbox"/> 1LG <input checked="" type="checkbox"/> LL | Network Options Switch impedance: 1e-005 + j 0.0001 Line capacitance emulation level: Normal Ignore phase shift: No <input type="button" value="Edit"/> |
| For X/R Calculation, use <input checked="" type="radio"/> Separate X-only, R-only networks <input type="radio"/> Complex impedance network | Fault Options Prefault Voltage: Flat 1.05 p.u. Generator reactance: Subtransient MOV iteration: Yes Enforce gen. curr. limit: No Ignore in short circuit: load, xformer line shunt <input type="button" value="Edit"/> |
| In 1LG faults, allow up to 15% higher rating for <input type="checkbox"/> Symmetrical current rated <input type="checkbox"/> Total current rated breakers | ANSI X/R Ratio Parameters Assume Z2=Z1: Yes If X is 0 use: 0.0001 If X is 0 use: min (X / g, Rc) Rc = 1. Typical X/R ratio (g) = 80 for generator 50 for transformers 50 for reactors 10 for others <input type="button" value="Edit"/> |
| Force voltage range factor K=1 in checking <input checked="" type="checkbox"/> Symmetrical-current rated breakers with max design kV 121. or higher <input type="checkbox"/> Total-current rated breakers with max design kV 121. or higher | |
| Misc. Options <input type="checkbox"/> Apply scaling factor F to the calculated breaker interrupting duty: <input type="radio"/> F = operating kV / nominal bus kV <input type="radio"/> F = operating kV / pre-fault bus kV <input type="checkbox"/> Set breaker operating kV equal to flat pre-fault voltage profile p.u. <input checked="" type="checkbox"/> Treat all sources as "Remote" <input type="checkbox"/> Ignore all reclosing settings <input type="checkbox"/> Show in report all faults simulated for breaker duty calculation <input type="checkbox"/> Compute breaker duty for out-of-service protected equipment | |
| <input type="button" value="Save"/> <input type="button" value="Load"/> | <input type="button" value="OK"/> <input type="button" value="Cancel"/> <input type="button" value="Help"/> |

7.3 Results

The following table shows the short circuit duty at each National Grid transmission substation (69 kV and above) in Western Massachusetts, following the additional of all 252 MW of DER associated with Group 3. The table includes the maximum short circuit current in Percentage (Duty_P) and Momentary Breaker Duty in Percentage (M_Duty_P) generated by the ASPEN breaker rating module for all 69 kV and above circuit breakers in Western Massachusetts.

The results show that the short circuit currents are less than 95% of the interrupting capability for all transmission breakers in the study area. Therefore, the PV inverters in Group 3 do not cause any breaker in the system to become overdutied.

Table 33 - ASPEN short circuit Results – Post Group 1 + 2 +3 DER

| BUS | Breaker | DUTY A (Maximum short ckt Amps) | BKR_CAPA (Amps) | DUTY P (%) | M DUTY A (Amps) | M BKR CAPA (Amps) | M DUTY P (%) | 3LG_AMPS | 1LG_AMPS | 2LG_AMPS | LL_AMPS |
|--------------------|-----------------|------------------------------------|-----------------|---------------|--------------------|----------------------|-----------------|----------|----------|----------|---------|
| AYER 115kV | AYER 137 | 16030.5 | 40000 | 40.1 | 23886 | 64000 | 37.3 | 20311 | 15181.8 | 19305.5 | 17526.4 |
| BEAR SWAMP 115.kV | BEAR SWP 131 | 24167.9 | 50000 | 48.3 | 36869.3 | 80000 | 46.1 | 23019.6 | 21923.4 | 22604.4 | 18959.1 |
| BEAR SWAMP 115.kV | BEAR SWP 197 | 24167.9 | 50000 | 48.3 | 36869.3 | 80000 | 46.1 | 23019.6 | 21923.4 | 22604.4 | 18959.1 |
| BEAR SWAMP 230.kV | BEARSW 1205E | 14306.9 | 63000 | 22.7 | 20816.3 | 100800 | 20.7 | 14204.7 | 14236.7 | 14491.6 | 11345.2 |
| BEAR SWAMP 230.kV | BEARSW 2205E | 14306.9 | 63000 | 22.7 | 20816.3 | 100800 | 20.7 | 14204.7 | 14236.7 | 14491.6 | 11345.2 |
| | | | | | | | | | | | |
| CHESTNUT HIL 69.kV | Proxy - 69kv | 2823.6 | 40000 | 7.1 | 2954.2 | 64000 | 4.6 | 2823.6 | 1680.5 | 2617.2 | 2474.3 |
| Crystal Lake 69.kV | Proxy - 69kv | 4104.1 | 31500 | 13 | 4509 | 50400 | 8.9 | 4104.1 | 2437.6 | 3802.6 | 3571.2 |
| DEERFIELD 4 69.kV | Proxy - 69kv | 10090.3 | 40000 | 25.2 | 13825.8 | 64000 | 21.6 | 10090.3 | 8435.9 | 9693.4 | 8466.7 |
| E LONGMDW 14 69.kV | Proxy - 69kv | 3229.6 | 40000 | 8.1 | 3868.5 | 64000 | 6 | 3229.6 | 1590.7 | 2922.4 | 2821 |
| E LONGMDW 15 69.kV | Proxy - 69kv | 4170.9 | 40000 | 10.4 | 6073.4 | 64000 | 9.5 | 4170.9 | 3698.4 | 4046.1 | 3592.7 |
| FLAGG POND 115.kV | 1135 | 17165.8 | 20000 | 85.8 | 23407.7 | 32000 | 73.1 | 17165.8 | 12456 | 15487 | 14501.6 |
| FLAGG POND 115.kV | 1136 | 17165.8 | 20000 | 85.8 | 23407.7 | 32000 | 73.1 | 17165.8 | 12456 | 15487 | 14501.6 |
| FLAGG POND 115.kV | 1235 | 12722.7 | 20924.4 | 60.8 | 17137.7 | 33479.1 | 51.2 | 17165.8 | 12456 | 15487 | 14501.6 |
| FLAGG POND 115.kV | 1236 | 12722.7 | 36444.4 | 34.9 | 17137.7 | 58311.1 | 29.4 | 17165.8 | 12456 | 15487 | 14501.6 |
| FLAGG POND 115.kV | 2135 | 12722.7 | 18884.4 | 67.4 | 17137.7 | 30215.1 | 56.7 | 17165.8 | 12456 | 15487 | 14501.6 |
| FLAGG POND 115.kV | 2136 | 17165.8 | 20000 | 85.8 | 23407.7 | 32000 | 73.1 | 17165.8 | 12456 | 15487 | 14501.6 |

| BUS | Breaker | DUTY A (Maximum short ckt Amps) | BKR_CAPA (Amps) | DUTY P (%) | M DUTY A (Amps) | M BKR CAPA (Amps) | M DUTY P (%) | 3LG_AMPS | 1LG_AMPS | 2LG_AMPS | LL_AMPS |
|------------------|-----------------|------------------------------------|-----------------|---------------|--------------------|----------------------|-----------------|----------|----------|----------|---------|
| HARRIMAN 69 kV | Proxy - 69kv | 7396.6 | 40000 | 18.5 | 11298 | 64000 | 17.7 | 7278.6 | 7354.7 | 7396.6 | 6184.9 |
| HARRIMAN 115.kV | 115BT | 15632.9 | 40000 | 39.1 | 22648.3 | 64000 | 35.4 | 15632.9 | 11759.7 | 14439.4 | 13195.1 |
| HARRIMAN 115.kV | HARRIM 3810 | 14752.8 | 40000 | 36.9 | 21206.6 | 64000 | 33.1 | 15632.9 | 11759.7 | 14439.4 | 13195.1 |
| HARRIMAN 115.kV | HARRIM A127 | 13721.1 | 40000 | 34.3 | 20070.4 | 64000 | 31.4 | 15632.9 | 11759.7 | 14439.4 | 13195.1 |
| HARRIMAN 115.kV | HARRIM B128 | 14514.7 | 40000 | 36.3 | 21166.7 | 64000 | 33.1 | 15632.9 | 11759.7 | 14439.4 | 13195.1 |
| HARRIMAN 115.kV | HARRIM Y177 | 13919.7 | 40000 | 34.8 | 20216.5 | 64000 | 31.6 | 15632.9 | 11759.7 | 14439.4 | 13195.1 |
| Harrington 69.kV | Proxy - 69kv | 9010.6 | 40000 | 22.5 | 11228.6 | 64000 | 17.5 | 9010.6 | 5774.6 | 8186 | 7596.7 |
| MEADOW ST 69.kV | Proxy - 69kv | 10415.2 | 31500 | 33.1 | 13036.9 | 50400 | 25.9 | 10415.2 | 5931.4 | 9178.1 | 8711.6 |

| BUS | Breaker | DUTY A (Maximum short ckt Amps) | BKR_CAPA (Amps) | DUTY P (%) | M DUTY A (Amps) | M BKR CAPA (Amps) | M DUTY P (%) | 3LG_AMPS | 1LG_AMPS | 2LG_AMPS | LL_AMPS |
|--------------------|-----------------|------------------------------------|-----------------|---------------|--------------------|----------------------|-----------------|----------|----------|----------|---------|
| | | | | | | | | | | | |
| MILLBURY5 B1 69 kV | Proxy - 69kv | 20323 | 31500 | 64.5 | 30826.8 | 50400 | 61.2 | 20323 | 19321.5 | 19873.1 | 17228.9 |
| | | | | | | | | | | | |
| OTTER RIV 1 69 kV | Proxy - 69kv | 3143.9 | 22000 | 14.3 | 3275.3 | 35200 | 9.3 | 3143.9 | 2051.3 | 2886 | 2759.1 |
| PALMER 69 kV | Proxy - 69kv | 14900.8 | 31500 | 47.3 | 22943 | 50400 | 45.5 | 14900.8 | 13192.6 | 14155.5 | 12659.6 |
| PALMER 115 115 kV | PALMER 176T | 15499.7 | 40000 | 38.7 | 22992.3 | 64000 | 35.9 | 15499.7 | 11411.5 | 14107 | 13187.4 |
| PALMER 115 115 kV | PALMER 7075 | 12114.1 | 40000 | 30.3 | 18031.3 | 64000 | 28.2 | 15499.7 | 11411.5 | 14107 | 13187.4 |
| PALMER 115 115 kV | PALMER R170 | 15499.7 | 40000 | 38.7 | 22992.3 | 64000 | 35.9 | 15499.7 | 11411.5 | 14107 | 13187.4 |
| PALMER 115 115 kV | PALMER W175 | 15499.7 | 40000 | 38.7 | 22992.3 | 64000 | 35.9 | 15499.7 | 11411.5 | 14107 | 13187.4 |
| PALMER 115 115 kV | PALMER X176 | 15337.5 | 40000 | 38.3 | 22778 | 64000 | 35.6 | 15499.7 | 11411.5 | 14107 | 13187.4 |
| PRATTS 115 115 kV | PRATTSJ 1110 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ 2110 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ 3741 | 29129.3 | 40000 | 72.8 | 41420.6 | 64000 | 64.7 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ 3842 | 28691.1 | 40000 | 71.7 | 40622 | 64000 | 63.5 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ 4A | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ 801 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |

| BUS | Breaker | DUTY A (Maximum short ckt Amps) | BKR_CAPA (Amps) | DUTY P (%) | M DUTY A (Amps) | M BKR CAPA (Amps) | M DUTY P (%) | 3LG_AMPS | 1LG_AMPS | 2LG_AMPS | LL_AMPS |
|---------------------|--------------|------------------------------------|-----------------|---------------|--------------------|----------------------|-----------------|----------|----------|----------|---------|
| PRATTS 115 115 kV | PRATTSJ 802 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ I135 | 31300.6 | 40000 | 78.3 | 44923.4 | 64000 | 70.2 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ J136 | 31317 | 40000 | 78.3 | 44947 | 64000 | 70.2 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ K137 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ L138 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ O141 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 115 115 kV | PRATTSJ P142 | 31827.2 | 40000 | 79.6 | 45641.3 | 64000 | 71.3 | 31827.2 | 24873.2 | 29884.6 | 27369.1 |
| PRATTS 230 230 kV | Pratts E205E | 7383.7 | 50000 | 14.8 | 11329.1 | 80000 | 14.2 | 9289.3 | 8252.5 | 8974 | 7953.1 |
| PRATTS JCT 1 69.kV | Proxy - 69kv | 26782.7 | 31500 | 85 | 39834.9 | 50400 | 79 | 26782.7 | 25112.5 | 26254.5 | 22989.3 |
| SEARSBURG 69.kV | Proxy - 69kv | 5746.1 | 40000 | 14.4 | 8268.6 | 64000 | 12.9 | 5746.1 | 4584.6 | 5382.2 | 4928.6 |
| SHUTESBRY E5 69.kV | Proxy - 69kv | 4237.8 | 31500 | 13.5 | 5114.8 | 50400 | 10.1 | 4237.8 | 2281.2 | 3687.6 | 3548.6 |
| Stafford st 115.kV | Proxy | 18799.6 | 40000 | 47 | 25829.4 | 64000 | 40.4 | 18799.6 | 11232.1 | 17131.6 | 16204.3 |
| VERNON 115.kV | K186 | 26529.4 | 40000 | 66.3 | 41305.5 | 64000 | 64.5 | 25824.7 | 25137.7 | 25990.5 | 21146.5 |
| VERNON 115.kV | K40 | 26529.4 | 40000 | 66.3 | 41305.5 | 64000 | 64.5 | 25824.7 | 25137.7 | 25990.5 | 21146.5 |
| VERNON 115.kV | KT1 | 26529.4 | 40000 | 66.3 | 41305.5 | 64000 | 64.5 | 25824.7 | 25137.7 | 25990.5 | 21146.5 |
| VERNON 115.kV | KTB1-B1 | 23286.6 | 40000 | 58.2 | 35581.9 | 64000 | 55.6 | 25824.7 | 25137.7 | 25990.5 | 21146.5 |
| VERNON 115.kV | KTB2-B1 | 26529.4 | 40000 | 66.3 | 41305.5 | 64000 | 64.5 | 25824.7 | 25137.7 | 25990.5 | 21146.5 |
| VERNON 1 69.kV | Proxy - 69kv | 5764.3 | 40000 | 14.4 | 7680 | 64000 | 12 | 5233.2 | 5535.9 | 5764.3 | 4425.4 |
| WARE 69.kV | Proxy - 69kv | 10293 | 31500 | 32.7 | 13232.8 | 50400 | 26.3 | 10293 | 5170 | 8897.3 | 8638.9 |
| West Hampden 115.kV | 1205 | 14358.4 | 40000 | 35.9 | 21013.7 | 64000 | 32.8 | 14358.4 | 10683.9 | 13280.9 | 12185.6 |
| West Hampden 115.kV | 1976 | 14358.4 | 40000 | 35.9 | 21013.7 | 64000 | 32.8 | 14358.4 | 10683.9 | 13280.9 | 12185.6 |
| West Hampden 115.kV | 3T-05 | 14331.8 | 40000 | 35.8 | 20974.8 | 64000 | 32.8 | 14358.4 | 10683.9 | 13280.9 | 12185.6 |
| West Hampden 115.kV | 70-76 | 11870.2 | 40000 | 29.7 | 17336.8 | 64000 | 27.1 | 14358.4 | 10683.9 | 13280.9 | 12185.6 |
| West Hampden 115.kV | Proxy 1 | 14358.4 | 40000 | 35.9 | 21013.7 | 64000 | 32.8 | 14358.4 | 10683.9 | 13280.9 | 12185.6 |
| West Hampden 115.kV | R170 | 14358.4 | 40000 | 35.9 | 21013.7 | 64000 | 32.8 | 14358.4 | 10683.9 | 13280.9 | 12185.6 |

| | |
|-------------|---|
| BUS | Breaker bus name and nominal kV |
| BREAKERS | Breaker name |
| RATINGTYPE | Breaker rating type: S for symmetrical current rated; T for total current rated |
| DUTY_P | Interrupting duty in percent |
| DUTY_A | Interrupting current in amps |
| BKR_CAPA | Calculated interrupting capacity in amps |
| M_DUTY_P | Momentary duty for total-current rated breakers and close-and-latch duty for symmetrical-current rated breakers in percent |
| M_DUTY_A | Momentary duty for total-current rated breakers and close-and-latch duty for symmetrical-current rated breakers in amps |
| M_BKR_CAPA | Calculated momentary capacity of total current rated breakers and close-and-latch capacity for symmetrical current rated breakers in amps |
| MAX_SC_CASE | Fault with maximum short circuit interrupting current |
| ISC | Breaker short circuit current in amps |
| ANSI_X/R | ANSI X/R ratio |
| FLAG | Rating flag, interrupting duty |
| FLAG_M | Rating flag, momentary (close-and-latch) duty |
| 3LG_AMPS | Maximum 3LG fault current at breaker bus |
| 3LG_X/R | ANSI X/R ratio in 3LG fault at breaker bus |
| 2LG_AMPS | Maximum 2LG fault current at breaker bus |
| 2LG_X/R | ANSI X/R ratio in 2LG fault at breaker bus |
| 1LG_AMPS | Maximum 1LG fault current at breaker bus |
| 1LG_X/R | ANSI X/R ratio in 1LG fault at breaker bus |
| LL_AMPS | Maximum LL fault current at breaker bus |
| LL_X/R | ANSI X/R ratio in LL fault at breaker bus |

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This appendix has been redacted for Critical Energy/
Electric Infrastructure Information (CEII).

Appendix A - Steady State Base Case Summaries

Note:

Base Case Summaries in Appendix A are for the transmission system prior to the dispatch of
Group 1,2 and 3 DER

This appendix has been redacted for Critical Energy/
Electric Infrastructure Information (CEII).

Appendix B – Stability Case Summaries

Appendix C - Stability Models (IDEV + DYR files) for Group 3 DER Greater Than or Equal To 5MW

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IDV File – 100% PV + BESS Discharging

//NEP-22-G03-034:

BAT_SPLT,113082,930822,'BARRE-GSU', 13.8
BAT_BRANCH_CHNG,113082,930822,'1',,,,,,0.030789,0.024765,,,,,
BAT_SPLT,930822,930821,'BARRE-INV', 0.6
BAT_BUS_CHNG_3,930821,2,,,,,
BAT_TWO_WINDING_DATA_4,930822,930821,'2',1,930822,600,0,0,0,33,0,930822,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,930821,930822,'2',,,,,,2,, 0.009450, 0.056720, 8.0,,,,," " "
BAT_PURGBRN,930821,930822,'1'
BAT_MBIDBRN,930821,930822,'2','1'
BAT_PLANT_DATA,930821,0, 1.0, 100.0
BAT_MACHINE_DATA_2,930821,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,930821,'D3',,,,,,1, 8.0,,0,0,0,0, 8.0,-8.0, 8.0,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-036:

BAT_SPLT,113396,933962,'Cryst-GSU', 13.8
BAT_BRANCH_CHNG,113396,933962,'1',,,,,,0.011195,0.006297,,,,,
BAT_SPLT,933962,933961,'Cryst-INV', 0.6
BAT_BUS_CHNG_3,933961,2,,,,,
BAT_TWO_WINDING_DATA_4,933962,933961,'2',1,933962,600,0,0,0,33,0,933962,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,933961,933962,'2',,,,,,2,, 0.009450, 0.056720, 8.0,,,,," " "
BAT_PURGBRN,933961,933962,'1'
BAT_MBIDBRN,933961,933962,'2','1'
BAT_PLANT_DATA,933961,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933961,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933961,'D3',,,,,,1, 8.0,,0,0,0,0, 8.0,-5.2, 8.0,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-038:

BAT_SPLT,113395,933952,'EWINC-GSU', 13.8
BAT_BRANCH_CHNG,113395,933952,'1',,,,,,0.002457,0.001382,,,,,
BAT_SPLT,933952,933951,'EWINC-INV', 0.6
BAT_BUS_CHNG_3,933951,2,,,,,
BAT_TWO_WINDING_DATA_4,933952,933951,'2',1,933952,600,0,0,0,33,0,933952,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,933951,933952,'2',,,,,,2,, 0.009450, 0.056720, 9.4,,,,," " "
BAT_PURGBRN,933951,933952,'1'
BAT_MBIDBRN,933951,933952,'2','1'
BAT_PLANT_DATA,933951,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933951,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933951,'D3',,,,,,1, 9.4,,0,0,0,0, 9.4,-4.6, 9.4,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-039:

BAT_SPLT,113395,993952,'EWINC2-GSU', 13.8
BAT_BRANCH_CHNG,113395,993952,'1',,,,,,0.001785,0.001004,,,,,
BAT_SPLT,993952,993951,'EWINC2-INV', 0.6
BAT_BUS_CHNG_3,993951,2,,,,,
BAT_TWO_WINDING_DATA_4,993952,993951,'2',1,993952,600,0,0,0,33,0,993952,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,993951,993952,'2',,,,,,2,, 0.009450, 0.056720, 5.5,,,,," " "
BAT_PURGBRN,993951,993952,'1'
BAT_MBIDBRN,993951,993952,'2','1'
BAT_PLANT_DATA,993951,0, 1.0, 100.0
BAT_MACHINE_DATA_2,993951,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,993951,'D3',,,,,,1, 5.5,,0,0,0,0, 5.5,-4.2, 5.5,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-029:

BAT_SPLT,113070,930702,'LASHA-GSU', 13.2
BAT_BRANCH_CHNG,113070,930702,'1',,,,,,0.005257,0.002957,,,,,
BAT_SPLT,930702,930701,'LASHA-INV', 0.6
BAT_BUS_CHNG_3,930701,2,,,,,

BAT_TWO_WINDING_DATA_4,930702,930701,'2',1,930702,600,0,0,0,33,0,930702,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,930701,930702,'2',,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,, " " " "
BAT_PURGBRN,930701,930702,'1'
BAT_MBIDBRN,930701,930702,'2','1'
BAT_PLANT_DATA,930701,0, 1.0, 100.0
BAT_MACHINE_DATA_2,930701,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,930701,'D3',,,,,,1, 10.0,,0,0,0,0, 10.0,-7.0, 10.0,,0.1,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-008:

BAT_SPLT,113377,933772,'LAURL-GSU', 13.8
BAT_BRANCH_CHNG,113377,933772,'1',,,,,,0.010658,0.008573,,,,,,,,;
BAT_SPLT,933772,933771,'LAURL-INV', 0.6
BAT_BUS_CHNG_3,933771,2,,,,,,,,;
BAT_TWO_WINDING_DATA_4,933772,933771,'2',1,933772,600,0,0,0,33,0,933772,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,933771,933772,'2',,,,,,,,,,2,, 0.009450, 0.056720, 8.0,,,,,,,,, " " " "
BAT_PURGBRN,933771,933772,'1'
BAT_MBIDBRN,933771,933772,'2','1'
BAT_PLANT_DATA,933771,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933771,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933771,'D3',,,,,,1, 8.0,,0,0,0,0, 8.0,-4.4, 8.0,,0.1,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-009:

BAT_SPLT,113392,933922,'MILLB-GSU', 13.8
BAT_BRANCH_CHNG,113392,933922,'1',,,,,,0.004054,0.00228,,,,,,,,;
BAT_SPLT,933922,933921,'MILLB-INV', 0.6
BAT_BUS_CHNG_3,933921,2,,,,,,,,;
BAT_TWO_WINDING_DATA_4,933922,933921,'2',1,933922,600,0,0,0,33,0,933922,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,933921,933922,'2',,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,, " " " "
BAT_PURGBRN,933921,933922,'1'
BAT_MBIDBRN,933921,933922,'2','1'
BAT_PLANT_DATA,933921,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933921,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933921,'D3',,,,,,1, 10.0,,0,0,0,0, 10.0,-3.5, 10.0,,0.1,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-011:

BAT_SPLT,113388,933882,'NOXFO1-GSU', 13.2
BAT_BRANCH_CHNG,113388,933882,'1',,,,,,0.003861,0.003106,,,,,,,,;
BAT_SPLT,933882,933881,'NOXFO1-INV', 0.6
BAT_BUS_CHNG_3,933881,2,,,,,,,,;
BAT_TWO_WINDING_DATA_4,933882,933881,'2',1,933882,600,0,0,0,33,0,933882,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,933881,933882,'2',,,,,,,,,,2,, 0.009450, 0.056720, 8.0,,,,,,,,, " " " "
BAT_PURGBRN,933881,933882,'1'
BAT_MBIDBRN,933881,933882,'2','1'
BAT_PLANT_DATA,933881,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933881,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933881,'D3',,,,,,1, 8.0,,0,0,0,0, 8.0,-6.4, 8.0,,0.1,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-013:

BAT_SPLT,113388,993882,'NOXFO2-GSU', 13.2
BAT_BRANCH_CHNG,113388,993882,'1',,,,,,0.008745,0.007034,,,,,,,,;
BAT_SPLT,993882,993881,'NOXFO2-INV', 0.6
BAT_BUS_CHNG_3,993881,2,,,,,,,,;
BAT_TWO_WINDING_DATA_4,993882,993881,'2',1,993882,600,0,0,0,33,0,993882,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,993881,993882,'2',,,,,,,,,,2,, 0.009450, 0.056720, 5.6,,,,,,,,, " " " "
BAT_PURGBRN,993881,993882,'1'
BAT_MBIDBRN,993881,993882,'2','1'
BAT_PLANT_DATA,993881,0, 1.0, 100.0
BAT_MACHINE_DATA_2,993881,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,993881,'D3',,,,,,1, 5.6,,0,0,0,0, 5.6,-4.8, 5.6,,0.1,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-006:

BAT_SPLT,113383,933832,'PRATT-GSU', 13.8
BAT_BRANCH_CHNG,113383,933832,'1',,,,,,0.020017,0.011259,,,,,,,,;

BAT_SPLT,933832,933831,'PRATT-INV', 0.6
 BAT_BUS_CHNG 3,933831,2,,,,,,,,,;
 BAT_TWO_WINDING_DATA 4,933832,933831,'2',1,933832,600,0,0,0,33,0,933832,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG 4,933831,933832,'2',,,,,,,,,,2,, 0.009450, 0.056720, 6.0,,,,,,,,,,,,, " " " "
 BAT_PURGBRN,933831,933832,'1'
 BAT_MBIDBRN,933831,933832,'2','1'
 BAT_PLANT_DATA,933831,0, 1.0, 100.0
 BAT_MACHINE_DATA 2,933831,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG 2,933831,'D3',,,,,,1, 6.0,,0,0,0,0, 6.0,-4.5, 6.0,,0.1,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-041:
 BAT_SPLT,113084,930842,'ROYAL-GSU', 13.8
 BAT_BRANCH_CHNG 113084,930842,'1',,,,,,0.00271,0.00152,,,,,,,,,;
 BAT_SPLT,930842,930841,'ROYAL-INV', 0.6
 BAT_BUS_CHNG 3,930841,2,,,,,,,,,;
 BAT_TWO_WINDING_DATA 4,930842,930841,'2',1,930842,600,0,0,0,33,0,930842,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG 4,930841,930842,'2',,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,, " " " "
 BAT_PURGBRN,930841,930842,'1'
 BAT_MBIDBRN,930841,930842,'2','1'
 BAT_PLANT_DATA,930841,0, 1.0, 100.0
 BAT_MACHINE_DATA 2,930841,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG 2,930841,'D3',,,,,,1, 5.0,,0,0,0,0, 5.0,0,0, 5.0,,0.1,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-015:
 BAT_SPLT,113389,933892,'SNOW1-GSU', 13.2
 BAT_BRANCH_CHNG 113389,933892,'1',,,,,,0.0119375,0.003094,,,,,,,,,;
 BAT_SPLT,933892,933891,'SNOW1-INV', 0.6
 BAT_BUS_CHNG 3,933891,2,,,,,,,,,;
 BAT_TWO_WINDING_DATA 4,933892,933891,'2',1,933892,600,0,0,0,33,0,933892,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG 4,933891,933892,'2',,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,, " " " "
 BAT_PURGBRN,933891,933892,'1'
 BAT_MBIDBRN,933891,933892,'2','1'
 BAT_PLANT_DATA,933891,0, 1.0, 100.0
 BAT_MACHINE_DATA 2,933891,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG 2,933891,'D3',,,,,,1, 5.0,,0,0,0,0, 5.0,-2.5, 5.0,,0.1,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-016:
 BAT_SPLT,113389,993892,'SNOW2-GSU', 13.2
 BAT_BRANCH_CHNG 113389,993892,'1',,,,,,0.01416,0.00797,,,,,,,,,;
 BAT_SPLT,993892,993891,'SNOW2-INV', 0.6
 BAT_BUS_CHNG 3,993891,2,,,,,,,,,;
 BAT_TWO_WINDING_DATA 4,993892,993891,'2',1,993892,600,0,0,0,33,0,993892,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG 4,993891,993892,'2',,,,,,,,,,2,, 0.009450, 0.056720, 5.5,,,,,,,,,,,,, " " " "
 BAT_PURGBRN,993891,993892,'1'
 BAT_MBIDBRN,993891,993892,'2','1'
 BAT_PLANT_DATA,993891,0, 1.0, 100.0
 BAT_MACHINE_DATA 2,993891,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG 2,993891,'D3',,,,,,1, 5.5,,0,0,0,0, 5.5,-6.5, 5.5,,0.1,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-017:
 BAT_SPLT,113389,983892,'SNOW3-GSU', 13.2
 BAT_BRANCH_CHNG 113389,983892,'1',,,,,,0.0119375,0.003094,,,,,,,,,;
 BAT_SPLT,983892,983891,'SNOW3-INV', 0.6
 BAT_BUS_CHNG 3,983891,2,,,,,,,,,;
 BAT_TWO_WINDING_DATA 4,983892,983891,'2',1,983892,600,0,0,0,33,0,983892,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG 4,983891,983892,'2',,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,, " " " "
 BAT_PURGBRN,983891,983892,'1'
 BAT_MBIDBRN,983891,983892,'2','1'
 BAT_PLANT_DATA,983891,0, 1.0, 100.0
 BAT_MACHINE_DATA 2,983891,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG 2,983891,'D3',,,,,,1, 5.0,,0,0,0,0, 5.0,-2.5, 5.0,,0.1,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-001:

BAT_SPLT,113363,933632,'STAFF-GSU', 13.8
 BAT_BRANCH_CHNG,113363,933632,'1',,,,,,0.00301169,0.00893508,,,,,,,,,,,,;
 BAT_SPLT,933632,933631,'STAFF-INV', 0.6
 BAT_BUS_CHNG_3,933631,2,,,,,,,,,,,,;
 BAT_TWO_WINDING_DATA_4,933632,933631,'2',1,933632,600,0,0,0,33,0,933632,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG_4,933631,933632,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,," " " "
 BAT_PURGBRN,933631,933632,'1'
 BAT_MBIDBRN,933631,933632,'2','1'
 BAT_PLANT_DATA,933631,0, 1.0, 100.0
 BAT_MACHINE_DATA_2,933631,'D3',1,600,0,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG_2,933631,'D3',,,,,,1, 5.0,,0,0,0,0, 5.0,-5.0, 5.0,,0.1,,,,,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-033:

BAT_SPLT,113368,933682,'TREAS-GSU', 13.8
 BAT_BRANCH_CHNG,113368,933682,'1',,,,,,0.002457,0.001382,,,,,,,,,,,,;
 BAT_SPLT,933682,933681,'TREAS-INV', 0.6
 BAT_BUS_CHNG_3,933681,2,,,,,,,,,,,,;
 BAT_TWO_WINDING_DATA_4,933682,933681,'2',1,933682,600,0,0,0,33,0,933682,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG_4,933681,933682,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,,,,,," " " "
 BAT_PURGBRN,933681,933682,'1'
 BAT_MBIDBRN,933681,933682,'2','1'
 BAT_PLANT_DATA,933681,0, 1.0, 100.0
 BAT_MACHINE_DATA_2,933681,'D3',1,600,0,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG_2,933681,'D3',,,,,,1, 10.0,,0,0,0,0, 10.0,-5.0, 10.0,,0.1,,,,,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-020:

BAT_SPLT,113390,933902,'WCHAR-GSU', 13.2
 BAT_BRANCH_CHNG,113390,933902,'1',,,,,,0.005624,0.003164,,,,,,,,,,,,;
 BAT_SPLT,933902,933901,'WCHAR-INV', 0.6
 BAT_BUS_CHNG_3,933901,2,,,,,,,,,,,,;
 BAT_TWO_WINDING_DATA_4,933902,933901,'2',1,933902,600,0,0,0,33,0,933902,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG_4,933901,933902,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,," " " "
 BAT_PURGBRN,933901,933902,'1'
 BAT_MBIDBRN,933901,933902,'2','1'
 BAT_PLANT_DATA,933901,0, 1.0, 100.0
 BAT_MACHINE_DATA_2,933901,'D3',1,600,0,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG_2,933901,'D3',,,,,,1, 5.0,,0,0,0,0, 5.0,-4.5, 5.0,,0.1,,,,,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-021:

BAT_SPLT,113390,993902,'WCHAR2-GSU', 13.2
 BAT_BRANCH_CHNG,113390,993902,'1',,,,,,0.00691,0.003887,,,,,,,,,,,,;
 BAT_SPLT,993902,993901,'WCHAR2-INV', 0.6
 BAT_BUS_CHNG_3,993901,2,,,,,,,,,,,,;
 BAT_TWO_WINDING_DATA_4,993902,993901,'2',1,993902,600,0,0,0,33,0,993902,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG_4,993901,993902,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,,,,,," " " "
 BAT_PURGBRN,993901,993902,'1'
 BAT_MBIDBRN,993901,993902,'2','1'
 BAT_PLANT_DATA,993901,0, 1.0, 100.0
 BAT_MACHINE_DATA_2,993901,'D3',1,600,0,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG_2,993901,'D3',,,,,,1, 10.0,,0,0,0,0, 10.0,-4.0, 10.0,,0.1,,,,,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-044:

BAT_SPLT,113085,930852,'WENDE1-GSU', 13.8
 BAT_BRANCH_CHNG,113085,930852,'1',,,,,,0.002625,0.001477,,,,,,,,,,,,;
 BAT_SPLT,930852,930851,'WENDE1-INV', 0.6
 BAT_BUS_CHNG_3,930851,2,,,,,,,,,,,,;
 BAT_TWO_WINDING_DATA_4,930852,930851,'2',1,930852,600,0,0,0,33,0,930852,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
 BAT_TWO_WINDING_CHNG_4,930851,930852,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 8.0,,,,,,,,,,,,," " " "
 BAT_PURGBRN,930851,930852,'1'
 BAT_MBIDBRN,930851,930852,'2','1'
 BAT_PLANT_DATA,930851,0, 1.0, 100.0
 BAT_MACHINE_DATA_2,930851,'D3',1,600,0,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG_2,930851,'D3',,,,,,1, 8.0,,0,0,0,0, 8.0,-7.2, 8.0,,0.1,,,,,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-043:

BAT_SPLT,113085,990852,'WENDE2-GSU', 13.8

BAT_BRANCH_CHNG,113085,990852,'1',,,,,,0.00271,0.001524,,,,,,,,,;

BAT_SPLT,990852,990851,'WENDE2-INV', 0.6

BAT_BUS_CHNG_3,990851,2,,,,,,,,,;

BAT_TWO_WINDING_DATA_4,990852,990851,'2',1,990852,600,0,0,0,33,0,990852,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0, 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "

BAT_TWO_WINDING_CHNG_4,990851,990852,'2',,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,,,,,," " " "

BAT_PURGBRN,990851,990852,'1'

BAT_MBIDBRN,990851,990852,'2','1'

BAT_PLANT_DATA,990851,0, 1.0, 100.0

BAT_MACHINE_DATA_2,990851,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0

BAT_MACHINE_CHNG_2,990851,'D3',,,,,,1, 10.0,,0,0,0,0, 10.0,-8.0, 10.0,,0.1,,,,,,,,,;

BAT_FDNS,1,0,0,1,1,0,0,0

IDV File – 26% PV + BESS Charging

//NEP-22-G03-034:

BAT_SPLT,113082,930822,'BARRE-GSU', 13.8
BAT_BRANCH_CHNG,113082,930822,'1',,,,,,0.030789,0.024765,,,,,
BAT_SPLT,930822,930821,'BARRE-INV', 0.6
BAT_BUS_CHNG_3,930821,2,,,,,
BAT_TWO_WINDING_DATA_4,930822,930821,'2',1,930822,600,0,0,0,33,0,930822,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,930821,930822,'2',,,,,,,2,, 0.009450, 0.056720, 8.0,,,,,, " " "
BAT_PURGBRN,930821,930822,'1'
BAT_MBIDBRN,930821,930822,'2','1'
BAT_PLANT_DATA,930821,0, 1.0, 100.0
BAT_MACHINE_DATA_2,930821,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,930821,'D3',,,,,,1, -8.0,,0,0,0,0, 8.0,-8.0, 8.0,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-036:

BAT_SPLT,113396,933962,'Cryst-GSU', 13.8
BAT_BRANCH_CHNG,113396,933962,'1',,,,,,0.011195,0.006297,,,,,
BAT_SPLT,933962,933961,'Cryst-INV', 0.6
BAT_BUS_CHNG_3,933961,2,,,,,
BAT_TWO_WINDING_DATA_4,933962,933961,'2',1,933962,600,0,0,0,33,0,933962,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,933961,933962,'2',,,,,,,2,, 0.009450, 0.056720, 8.0,,,,,, " " "
BAT_PURGBRN,933961,933962,'1'
BAT_MBIDBRN,933961,933962,'2','1'
BAT_PLANT_DATA,933961,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933961,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933961,'D3',,,,,,1, -5.2,,0,0,0,0, 8.0,-5.2, 8.0,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-038:

BAT_SPLT,113395,933952,'EWINC-GSU', 13.8
BAT_BRANCH_CHNG,113395,933952,'1',,,,,,0.002457,0.001382,,,,,
BAT_SPLT,933952,933951,'EWINC-INV', 0.6
BAT_BUS_CHNG_3,933951,2,,,,,
BAT_TWO_WINDING_DATA_4,933952,933951,'2',1,933952,600,0,0,0,33,0,933952,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,933951,933952,'2',,,,,,,2,, 0.009450, 0.056720, 9.4,,,,,, " " "
BAT_PURGBRN,933951,933952,'1'
BAT_MBIDBRN,933951,933952,'2','1'
BAT_PLANT_DATA,933951,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933951,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933951,'D3',,,,,,1, -4.6,,0,0,0,0, 9.4,-4.6, 9.4,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-039:

BAT_SPLT,113395,993952,'EWINC2-GSU', 13.8
BAT_BRANCH_CHNG,113395,993952,'1',,,,,,0.001785,0.001004,,,,,
BAT_SPLT,993952,993951,'EWINC2-INV', 0.6
BAT_BUS_CHNG_3,993951,2,,,,,
BAT_TWO_WINDING_DATA_4,993952,993951,'2',1,993952,600,0,0,0,33,0,993952,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,993951,993952,'2',,,,,,,2,, 0.009450, 0.056720, 5.5,,,,,, " " "
BAT_PURGBRN,993951,993952,'1'
BAT_MBIDBRN,993951,993952,'2','1'
BAT_PLANT_DATA,993951,0, 1.0, 100.0
BAT_MACHINE_DATA_2,993951,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,993951,'D3',,,,,,1, -4.2,,0,0,0,0, 5.5,-4.2, 5.5,,0.1,,,,,
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-029:

BAT_SPLT,113070,930702,'LASHA-GSU', 13.2
BAT_BRANCH_CHNG,113070,930702,'1',,,,,,0.005257,0.002957,,,,,
BAT_SPLT,930702,930701,'LASHA-INV', 0.6
BAT_BUS_CHNG_3,930701,2,,,,,
BAT_TWO_WINDING_DATA_4,930702,930701,'2',1,930702,600,0,0,0,33,0,930702,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " "
BAT_TWO_WINDING_CHNG_4,930701,930702,'2',,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,, " " "
BAT_PURGBRN,930701,930702,'1'
BAT_MBIDBRN,930701,930702,'2','1'

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BAT_PLANT_DATA,930701,0, 1.0, 100.0
BAT_MACHINE_DATA 2,930701,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG 2,930701,'D3',,,,,,1, -7.0,,0.0,0.0, 10.0,-7.0, 10.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-008:
BAT_SPLT,113377,933772,'LAURL-GSU', 13.8
BAT_BRANCH_CHNG,113377,933772,'1',,,,,,0.010658,0.008573,,,,,;
BAT_SPLT,933772,933771,'LAURL-INV', 0.6
BAT_BUS_CHNG 3,933771,2,,,,,;
BAT_TWO_WINDING_DATA 4,933772,933771,'2',1,933772,600,0,0,0,33,0,933772,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG 4,933771,933772,'2',,,,,,2,, 0.009450, 0.056720, 8.0,,,,,," " "
BAT_PURGBRN,933771,933772,'1'
BAT_MBIDBRN,933771,933772,'2','1'
BAT_PLANT_DATA,933771,0, 1.0, 100.0
BAT_MACHINE_DATA 2,933771,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG 2,933771,'D3',,,,,,1, -4.4,,0.0,0.0, 8.0,-4.4, 8.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-009:
BAT_SPLT,113392,933922,'MILLB-GSU', 13.8
BAT_BRANCH_CHNG,113392,933922,'1',,,,,,0.004054,0.00228,,,,,;
BAT_SPLT,933922,933921,'MILLB-INV', 0.6
BAT_BUS_CHNG 3,933921,2,,,,,;
BAT_TWO_WINDING_DATA 4,933922,933921,'2',1,933922,600,0,0,0,33,0,933922,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG 4,933921,933922,'2',,,,,,2,, 0.009450, 0.056720, 10.0,,,,,," " "
BAT_PURGBRN,933921,933922,'1'
BAT_MBIDBRN,933921,933922,'2','1'
BAT_PLANT_DATA,933921,0, 1.0, 100.0
BAT_MACHINE_DATA 2,933921,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG 2,933921,'D3',,,,,,1, -3.5,,0.0,0.0, 10.0,-3.5, 10.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-011:
BAT_SPLT,113388,933882,'NOXFO1-GSU', 13.2
BAT_BRANCH_CHNG,113388,933882,'1',,,,,,0.003861,0.003106,,,,,;
BAT_SPLT,933882,933881,'NOXFO1-INV', 0.6
BAT_BUS_CHNG 3,933881,2,,,,,;
BAT_TWO_WINDING_DATA 4,933882,933881,'2',1,933882,600,0,0,0,33,0,933882,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG 4,933881,933882,'2',,,,,,2,, 0.009450, 0.056720, 8.0,,,,,," " "
BAT_PURGBRN,933881,933882,'1'
BAT_MBIDBRN,933881,933882,'2','1'
BAT_PLANT_DATA,933881,0, 1.0, 100.0
BAT_MACHINE_DATA 2,933881,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG 2,933881,'D3',,,,,,1, -6.4,,0.0,0.0, 8.0,-6.4, 8.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-013:
BAT_SPLT,113388,993882,'NOXFO2-GSU', 13.2
BAT_BRANCH_CHNG,113388,993882,'1',,,,,,0.008745,0.007034,,,,,;
BAT_SPLT,993882,993881,'NOXFO2-INV', 0.6
BAT_BUS_CHNG 3,993881,2,,,,,;
BAT_TWO_WINDING_DATA 4,993882,993881,'2',1,993882,600,0,0,0,33,0,993882,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG 4,993881,993882,'2',,,,,,2,, 0.009450, 0.056720, 5.6,,,,,," " "
BAT_PURGBRN,993881,993882,'1'
BAT_MBIDBRN,993881,993882,'2','1'
BAT_PLANT_DATA,993881,0, 1.0, 100.0
BAT_MACHINE_DATA 2,993881,'D3',1,600,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG 2,993881,'D3',,,,,,1, -4.8,,0.0,0.0, 5.6,-4.8, 5.6,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-006:
BAT_SPLT,113383,933832,'PRATT-GSU', 13.8
BAT_BRANCH_CHNG,113383,933832,'1',,,,,,0.020017,0.011259,,,,,;
BAT_SPLT,933832,933831,'PRATT-INV', 0.6
BAT_BUS_CHNG 3,933831,2,,,,,;
BAT_TWO_WINDING_DATA 4,933832,933831,'2',1,933832,600,0,0,0,33,0,933832,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG 4,933831,933832,'2',,,,,,2,, 0.009450, 0.056720, 6.0,,,,,," " "

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BAT_PURGBRN,933831,933832,'1'
BAT_MBIDBRN,933831,933832,'2','1'
BAT_PLANT_DATA,933831,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933831,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933831,'D3',,,,,,1, -4.5,,0.0,0.0, 6.0,-4.5, 6.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-041:
BAT_SPLT,113084,930842,'ROYAL-GSU', 13.8
BAT_BRANCH_CHNG,113084,930842,'1',,,,,,0.00271,0.00152,,,,,;
BAT_SPLT,930842,930841,'ROYAL-INV', 0.6
BAT_BUS_CHNG_3,930841,2,,,,,;
BAT_TWO_WINDING_DATA_4,930842,930841,'2',1,930842,600,0,0,0,33,0,930842,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG_4,930841,930842,'2',,,,,,2,, 0.009450, 0.056720, 5.0,,,,,," " "
BAT_PURGBRN,930841,930842,'1'
BAT_MBIDBRN,930841,930842,'2','1'
BAT_PLANT_DATA,930841,0, 1.0, 100.0
BAT_MACHINE_DATA_2,930841,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,930841,'D3',,,,,,1, 0.0,,0.0,0.0, 5.0,0.0, 5.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-015:
BAT_SPLT,113389,933892,'SNOW1-GSU', 13.2
BAT_BRANCH_CHNG,113389,933892,'1',,,,,,0.0119375,0.003094,,,,,;
BAT_SPLT,933892,933891,'SNOW1-INV', 0.6
BAT_BUS_CHNG_3,933891,2,,,,,;
BAT_TWO_WINDING_DATA_4,933892,933891,'2',1,933892,600,0,0,0,33,0,933892,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG_4,933891,933892,'2',,,,,,2,, 0.009450, 0.056720, 5.0,,,,,," " "
BAT_PURGBRN,933891,933892,'1'
BAT_MBIDBRN,933891,933892,'2','1'
BAT_PLANT_DATA,933891,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933891,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933891,'D3',,,,,,1, -2.5,,0.0,0.0, 5.0,-2.5, 5.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-016:
BAT_SPLT,113389,993892,'SNOW2-GSU', 13.2
BAT_BRANCH_CHNG,113389,993892,'1',,,,,,0.01416,0.00797,,,,,;
BAT_SPLT,993892,993891,'SNOW2-INV', 0.6
BAT_BUS_CHNG_3,993891,2,,,,,;
BAT_TWO_WINDING_DATA_4,993892,993891,'2',1,993892,600,0,0,0,33,0,993892,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG_4,993891,993892,'2',,,,,,2,, 0.009450, 0.056720, 5.5,,,,,," " "
BAT_PURGBRN,993891,993892,'1'
BAT_MBIDBRN,993891,993892,'2','1'
BAT_PLANT_DATA,993891,0, 1.0, 100.0
BAT_MACHINE_DATA_2,993891,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,993891,'D3',,,,,,1, -6.5,,0.0,0.0, 5.5,-6.5, 5.5,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-017:
BAT_SPLT,113389,983892,'SNOW3-GSU', 13.2
BAT_BRANCH_CHNG,113389,983892,'1',,,,,,0.0119375,0.003094,,,,,;
BAT_SPLT,983892,983891,'SNOW3-INV', 0.6
BAT_BUS_CHNG_3,983891,2,,,,,;
BAT_TWO_WINDING_DATA_4,983892,983891,'2',1,983892,600,0,0,0,33,0,983892,0,1,0,1,1,1,0.0, 0.0001, 100.0, 1.0,0.0,0.0, 1.0,0.0,0.0,0.0,0.0, 1.0,
1.0, 1.0, 1.0,0.0,0.0, 1.1, 0.9, 1.1, 0.9,0.0,0.0,0.0," " " "
BAT_TWO_WINDING_CHNG_4,983891,983892,'2',,,,,,2,, 0.009450, 0.056720, 5.0,,,,,," " "
BAT_PURGBRN,983891,983892,'1'
BAT_MBIDBRN,983891,983892,'2','1'
BAT_PLANT_DATA,983891,0, 1.0, 100.0
BAT_MACHINE_DATA_2,983891,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0.0, 1.0,0.0,0.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,983891,'D3',,,,,,1, -2.5,,0.0,0.0, 5.0,-2.5, 5.0,,0.1,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-001:
BAT_SPLT,113363,933632,'STAFF-GSU', 13.8
BAT_BRANCH_CHNG,113363,933632,'1',,,,,,0.00301169,0.00893508,,,,,;
BAT_SPLT,933632,933631,'STAFF-INV', 0.6
BAT_BUS_CHNG_3,933631,2,,,,,;

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BAT_TWO_WINDING_DATA_4,933632,933631,'2',1,933632,600,0,0,0,33,0,933632,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,933631,933632,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,, " " " "
BAT_PURGBRN,933631,933632,'1'
BAT_MBIDBRN,933631,933632,'2','1'
BAT_PLANT_DATA,933631,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933631,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933631,'D3',,,,,,1, -5.0,,0,0,0,0, 5.0,-5.0, 5.0,,0.1,,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-033:

BAT_SPLT,113368,933682,'TREAS-GSU', 13.8
BAT_BRANCH_CHNG,113368,933682,'1',,,,,,0.002457,0.001382,,,,,,,,,;
BAT_SPLT,933682,933681,'TREAS-INV', 0.6
BAT_BUS_CHNG_3,933681,2,,,,,,,,,;
BAT_TWO_WINDING_DATA_4,933682,933681,'2',1,933682,600,0,0,0,33,0,933682,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,933681,933682,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,,,,,, " " " "
BAT_PURGBRN,933681,933682,'1'
BAT_MBIDBRN,933681,933682,'2','1'
BAT_PLANT_DATA,933681,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933681,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933681,'D3',,,,,,1, -5.0,,0,0,0,0, 10.0,-5.0, 10.0,,0.1,,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-020:

BAT_SPLT,113390,933902,'WCHAR-GSU', 13.2
BAT_BRANCH_CHNG,113390,933902,'1',,,,,,0.005624,0.003164,,,,,,,,,;
BAT_SPLT,933902,933901,'WCHAR-INV', 0.6
BAT_BUS_CHNG_3,933901,2,,,,,,,,,;
BAT_TWO_WINDING_DATA_4,933902,933901,'2',1,933902,600,0,0,0,33,0,933902,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,933901,933902,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 5.0,,,,,,,,,,,,, " " " "
BAT_PURGBRN,933901,933902,'1'
BAT_MBIDBRN,933901,933902,'2','1'
BAT_PLANT_DATA,933901,0, 1.0, 100.0
BAT_MACHINE_DATA_2,933901,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,933901,'D3',,,,,,1, -4.5,,0,0,0,0, 5.0,-4.5, 5.0,,0.1,,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-021:

BAT_SPLT,113390,993902,'WCHAR2-GSU', 13.2
BAT_BRANCH_CHNG,113390,993902,'1',,,,,,0.00691,0.003887,,,,,,,,,;
BAT_SPLT,993902,993901,'WCHAR2-INV', 0.6
BAT_BUS_CHNG_3,993901,2,,,,,,,,,;
BAT_TWO_WINDING_DATA_4,993902,993901,'2',1,993902,600,0,0,0,33,0,993902,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,993901,993902,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,,,,,, " " " "
BAT_PURGBRN,993901,993902,'1'
BAT_MBIDBRN,993901,993902,'2','1'
BAT_PLANT_DATA,993901,0, 1.0, 100.0
BAT_MACHINE_DATA_2,993901,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,993901,'D3',,,,,,1, -4.0,,0,0,0,0, 10.0,-4.0, 10.0,,0.1,,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-044:

BAT_SPLT,113085,930852,'WENDE1-GSU', 13.8
BAT_BRANCH_CHNG,113085,930852,'1',,,,,,0.002625,0.001477,,,,,,,,,;
BAT_SPLT,930852,930851,'WENDE1-INV', 0.6
BAT_BUS_CHNG_3,930851,2,,,,,,,,,;
BAT_TWO_WINDING_DATA_4,930852,930851,'2',1,930852,600,0,0,0,33,0,930852,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," " " "
BAT_TWO_WINDING_CHNG_4,930851,930852,'2',,,,,,,,,,,,,,2,, 0.009450, 0.056720, 8.0,,,,,,,,,,,,, " " " "
BAT_PURGBRN,930851,930852,'1'
BAT_MBIDBRN,930851,930852,'2','1'
BAT_PLANT_DATA,930851,0, 1.0, 100.0
BAT_MACHINE_DATA_2,930851,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
BAT_MACHINE_CHNG_2,930851,'D3',,,,,,1, -7.2,,0,0,0,0, 8.0,-7.2, 8.0,,0.1,,,,,,,,,;
BAT_FDNS,1,0,0,1,1,0,0,0

//NEP-22-G03-043:

BAT_SPLT,113085,990852,'WENDE2-GSU', 13.8
BAT_BRANCH_CHNG,113085,990852,'1',,,,,,0.00271,0.001524,,,,,,,,,;

BAT_SPLT,990852,990851,'WENDE2-INV', 0.6
 BAT_BUS_CHNG 3,990851,2,,,,,,,,,;
 BAT_TWO_WINDING_DATA_4,990852,990851,'2',1,990852,600,0,0,0,33,0,990852,0,1,0,1,1,1,0,0, 0.0001, 100.0, 1.0,0,0,0,0, 1.0,0,0,0,0,0,0,0,0, 1.0,
 1.0, 1.0, 1.0,0,0,0,0, 1.1, 0.9, 1.1, 0.9,0,0,0,0,0,0," "," "
 BAT_TWO_WINDING_CHNG_4,990851,990852,'2',,,,,,,,,,2,, 0.009450, 0.056720, 10.0,,,,,,,,,,,,," "," "
 BAT_PURGBRN,990851,990852,'1'
 BAT_MBIDBRN,990851,990852,'2','1'
 BAT_PLANT_DATA,990851,0, 1.0, 100.0
 BAT_MACHINE_DATA_2,990851,'D3',1,600,0,0,0,0,0,0,0,0, 9999.0,-9999.0, 9999.0,-9999.0, 100.0,0,0, 1.0,0,0,0,0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0
 BAT_MACHINE_CHNG_2,990851,'D3',,,,,,1, -8.0,,0,0,0,0, 10.0,-8.0, 10.0,,0.1,,,,,,,,;
 BAT_FDNS,1,0,0,1,1,0,0,0

DYR File

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///NEP-22-G03-034
930821 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/930821 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

930821 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993082101 'VTGTPAT' 930821 930821 D3 -1 1.2 0.16 0.0 /
993082102 'VTGTPAT' 930821 930821 D3 -1 1.1 2 0.0 /
993082103 'VTGTPAT' 930821 930821 D3 0.5 5 1.1 0.0 /
993082104 'VTGTPAT' 930821 930821 D3 0.88 5 3 0.0 /
993082105 'FRQTPAT' 930821 930821 D3 56.5 100 0.16 0.0 /
993082106 'FRQTPAT' 930821 930821 D3 58.5 100 300 0.0 /
993082107 'FRQTPAT' 930821 930821 D3 -100 61.2 300 0.0 /
993082108 'FRQTPAT' 930821 930821 D3 -100 62 0.16 0.0 /

///NEP-22-G03-036
933961 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933961 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933961 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993396101 'VTGTPAT' 933961 933961 D3 -1 1.2 0.16 0.0 /
993396102 'VTGTPAT' 933961 933961 D3 -1 1.1 2 0.0 /
993396103 'VTGTPAT' 933961 933961 D3 0.5 5 1.1 0.0 /
993396104 'VTGTPAT' 933961 933961 D3 0.88 5 3 0.0 /
993396105 'FRQTPAT' 933961 933961 D3 56.5 100 0.16 0.0 /
993396106 'FRQTPAT' 933961 933961 D3 58.5 100 300 0.0 /
993396107 'FRQTPAT' 933961 933961 D3 -100 61.2 300 0.0 /
993396108 'FRQTPAT' 933961 933961 D3 -100 62 0.16 0.0 /

///NEP-22-G03-038
933951 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933951 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933951 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
```

0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993395101 'VTGTPAT' 933951 933951 D3 -1 1.2 0.16 0.0 /
993395102 'VTGTPAT' 933951 933951 D3 -1 1.1 2 0.0 /
993395103 'VTGTPAT' 933951 933951 D3 0.5 5 1.1 0.0 /
993395104 'VTGTPAT' 933951 933951 D3 0.88 5 3 0.0 /
993395105 'FRQTPAT' 933951 933951 D3 56.5 100 0.16 0.0 /
993395106 'FRQTPAT' 933951 933951 D3 58.5 100 300 0.0 /
993395107 'FRQTPAT' 933951 933951 D3 -100 61.2 300 0.0 /
993395108 'FRQTPAT' 933951 933951 D3 -100 62 0.16 0.0 /

///NEP-22-G03-039
993951 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/993951 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

993951 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

999395101 'VTGTPAT' 993951 993951 D3 -1 1.2 0.16 0.0 /
999395102 'VTGTPAT' 993951 993951 D3 -1 1.1 2 0.0 /
999395103 'VTGTPAT' 993951 993951 D3 0.5 5 1.1 0.0 /
999395104 'VTGTPAT' 993951 993951 D3 0.88 5 3 0.0 /
999395105 'FRQTPAT' 993951 993951 D3 56.5 100 0.16 0.0 /
999395106 'FRQTPAT' 993951 993951 D3 58.5 100 300 0.0 /
999395107 'FRQTPAT' 993951 993951 D3 -100 61.2 300 0.0 /
999395108 'FRQTPAT' 993951 993951 D3 -100 62 0.16 0.0 /

///NEP-22-G03-029
930701 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/930701 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

930701 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993070101 'VTGTPAT' 930701 930701 D3 -1 1.2 0.16 0.0 /
993070102 'VTGTPAT' 930701 930701 D3 -1 1.1 2 0.0 /
993070103 'VTGTPAT' 930701 930701 D3 0.5 5 1.1 0.0 /
993070104 'VTGTPAT' 930701 930701 D3 0.88 5 3 0.0 /
993070105 'FRQTPAT' 930701 930701 D3 56.5 100 0.16 0.0 /
993070106 'FRQTPAT' 930701 930701 D3 58.5 100 300 0.0 /
993070107 'FRQTPAT' 930701 930701 D3 -100 61.2 300 0.0 /
993070108 'FRQTPAT' 930701 930701 D3 -100 62 0.16 0.0 /

///NEP-22-G03-008
933771 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933771 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933771 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993377101 'VTGTPAT' 933771 933771 D3 -1 1.2 0.16 0.0 /
993377102 'VTGTPAT' 933771 933771 D3 -1 1.1 2 0.0 /
993377103 'VTGTPAT' 933771 933771 D3 0.5 5 1.1 0.0 /
993377104 'VTGTPAT' 933771 933771 D3 0.88 5 3 0.0 /
993377105 'FRQTPAT' 933771 933771 D3 56.5 100 0.16 0.0 /
993377106 'FRQTPAT' 933771 933771 D3 58.5 100 300 0.0 /
993377107 'FRQTPAT' 933771 933771 D3 -100 61.2 300 0.0 /
993377108 'FRQTPAT' 933771 933771 D3 -100 62 0.16 0.0 /

///NEP-22-G03-009

933921 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933921 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933921 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993392101 'VTGTPAT' 933921 933921 D3 -1 1.2 0.16 0.0 /
993392102 'VTGTPAT' 933921 933921 D3 -1 1.1 2 0.0 /
993392103 'VTGTPAT' 933921 933921 D3 0.5 5 1.1 0.0 /
993392104 'VTGTPAT' 933921 933921 D3 0.88 5 3 0.0 /
993392105 'FRQTPAT' 933921 933921 D3 56.5 100 0.16 0.0 /
993392106 'FRQTPAT' 933921 933921 D3 58.5 100 300 0.0 /
993392107 'FRQTPAT' 933921 933921 D3 -100 61.2 300 0.0 /
993392108 'FRQTPAT' 933921 933921 D3 -100 62 0.16 0.0 /

///NEP-22-G03-011

933881 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933881 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933881 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993388101 'VTGTPAT' 933881 933881 D3 -1 1.2 0.16 0.0 /
993388102 'VTGTPAT' 933881 933881 D3 -1 1.1 2 0.0 /
993388103 'VTGTPAT' 933881 933881 D3 0.5 5 1.1 0.0 /
993388104 'VTGTPAT' 933881 933881 D3 0.88 5 3 0.0 /
993388105 'FRQTPAT' 933881 933881 D3 56.5 100 0.16 0.0 /
993388106 'FRQTPAT' 933881 933881 D3 58.5 100 300 0.0 /
993388107 'FRQTPAT' 933881 933881 D3 -100 61.2 300 0.0 /
993388108 'FRQTPAT' 933881 933881 D3 -100 62 0.16 0.0 /

///NEP-22-G03-013

993881 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/993881 'REPCA1' D3

/1111 101 1111 '1' 1 0 1

/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0

/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

993881 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

0 1 0 0 1 0

0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0

0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9

0 0.02 99 -99 1 -1 1.2 0.02

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

999388101 'VTGTPAT' 993881 993881 D3 -1 1.2 0.16 0.0 /

999388102 'VTGTPAT' 993881 993881 D3 -1 1.1 2 0.0 /

999388103 'VTGTPAT' 993881 993881 D3 0.5 5 1.1 0.0 /

999388104 'VTGTPAT' 993881 993881 D3 0.88 5 3 0.0 /

999388105 'FRQTPAT' 993881 993881 D3 56.5 100 0.16 0.0 /

999388106 'FRQTPAT' 993881 993881 D3 58.5 100 300 0.0 /

999388107 'FRQTPAT' 993881 993881 D3 -100 61.2 300 0.0 /

999388108 'FRQTPAT' 993881 993881 D3 -100 62 0.16 0.0 /

///NEP-22-G03-006

933831 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1

0.02 0.02 99 -99 10.0 0.01 1.0/

/933831 'REPCA1' D3

/1111 101 1111 '1' 1 0 1

/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0

/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933831 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

0 1 0 0 1 0

0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0

0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9

0 0.02 99 -99 1 -1 1.2 0.02

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993383101 'VTGTPAT' 933831 933831 D3 -1 1.2 0.16 0.0 /

993383102 'VTGTPAT' 933831 933831 D3 -1 1.1 2 0.0 /

993383103 'VTGTPAT' 933831 933831 D3 0.5 5 1.1 0.0 /

993383104 'VTGTPAT' 933831 933831 D3 0.88 5 3 0.0 /

993383105 'FRQTPAT' 933831 933831 D3 56.5 100 0.16 0.0 /

993383106 'FRQTPAT' 933831 933831 D3 58.5 100 300 0.0 /

993383107 'FRQTPAT' 933831 933831 D3 -100 61.2 300 0.0 /

993383108 'FRQTPAT' 933831 933831 D3 -100 62 0.16 0.0 /

///NEP-22-G03-041

930841 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8

0 0

0.0200 0.0200 99.000 -99.000 10.000

0.0100 1.0000/

930841 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

0 0 0 0 0 0

0.8800 1.2000 0.0200 -0.1000 0.1000

1.0000 1.0000 -1.0000 0.0000 0.0000

0.0000 0.0000 0.0100 0.0000 0.0000

1.1000 0.9000 0.3000 5.0000 0.5000

0.0000 0.0000 0.0200 99.000 -99.000

1.0000 -1.0000 1.2000 0.0200

0.01 0.01 0.499 0.01 0.5 1.0 0.6 1.0 0.9 1.0 1.0 1.1 1.0 1.2 1.0 1.201 0.01 1.3 0.01

0.01 0.01 0.499 0.01 0.5 1.0 0.6 1.0 0.9 1.0 1.0 1.1 1.0 1.2 1.0 1.201 0.01 1.3 0.01

0.0000 0.0000 0.0000 0.0000 1.0000

0.5000 1.1000 0.0000/

993084101 'VTGTPAT' 930841 930841 D3 -1 1.2 0.16 0.0 /
993084102 'VTGTPAT' 930841 930841 D3 -1 1.1 2 0.0 /
993084103 'VTGTPAT' 930841 930841 D3 0.5 5 1.1 0.0 /
993084104 'VTGTPAT' 930841 930841 D3 0.88 5 3 0.0 /
993084105 'FRQTPAT' 930841 930841 D3 56.5 100 0.16 0.0 /
993084106 'FRQTPAT' 930841 930841 D3 58.5 100 300 0.0 /
993084107 'FRQTPAT' 930841 930841 D3 -100 61.2 300 0.0 /
993084108 'FRQTPAT' 930841 930841 D3 -100 62 0.16 0.0 /

///NEP-22-G03-015

933891 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933891 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933891 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993389101 'VTGTPAT' 933891 933891 D3 -1 1.2 0.16 0.0 /
993389102 'VTGTPAT' 933891 933891 D3 -1 1.1 2 0.0 /
993389103 'VTGTPAT' 933891 933891 D3 0.5 5 1.1 0.0 /
993389104 'VTGTPAT' 933891 933891 D3 0.88 5 3 0.0 /
993389105 'FRQTPAT' 933891 933891 D3 56.5 100 0.16 0.0 /
993389106 'FRQTPAT' 933891 933891 D3 58.5 100 300 0.0 /
993389107 'FRQTPAT' 933891 933891 D3 -100 61.2 300 0.0 /
993389108 'FRQTPAT' 933891 933891 D3 -100 62 0.16 0.0 /

///NEP-22-G03-016

993891 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/993891 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

993891 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

999389101 'VTGTPAT' 993891 993891 D3 -1 1.2 0.16 0.0 /
999389102 'VTGTPAT' 993891 993891 D3 -1 1.1 2 0.0 /
999389103 'VTGTPAT' 993891 993891 D3 0.5 5 1.1 0.0 /
999389104 'VTGTPAT' 993891 993891 D3 0.88 5 3 0.0 /
999389105 'FRQTPAT' 993891 993891 D3 56.5 100 0.16 0.0 /
999389106 'FRQTPAT' 993891 993891 D3 58.5 100 300 0.0 /
999389107 'FRQTPAT' 993891 993891 D3 -100 61.2 300 0.0 /
999389108 'FRQTPAT' 993891 993891 D3 -100 62 0.16 0.0 /

///NEP-22-G03-017

983891 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/983891 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

983891 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
 0 1 0 0 1 0
 0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
 0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
 0 0.02 99 -99 1 -1 1.2 0.02
 0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
 0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
 0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

998389101 'VTGTPAT' 983891 983891 D3 -1 1.2 0.16 0.0 /
 998389102 'VTGTPAT' 983891 983891 D3 -1 1.1 2 0.0 /
 998389103 'VTGTPAT' 983891 983891 D3 0.5 5 1.1 0.0 /
 998389104 'VTGTPAT' 983891 983891 D3 0.88 5 3 0.0 /
 998389105 'FRQTPAT' 983891 983891 D3 56.5 100 0.16 0.0 /
 998389106 'FRQTPAT' 983891 983891 D3 58.5 100 300 0.0 /
 998389107 'FRQTPAT' 983891 983891 D3 -100 61.2 300 0.0 /
 998389108 'FRQTPAT' 983891 983891 D3 -100 62 0.16 0.0 /

///NEP-22-G03-001

933631 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8

@! / ----- ICONS -----

@! / 1.RateFlag 2.PQpriority

0 0

@! / ----- CONS -----

@! / 1.Tg 2.Tflt 3.lqrmax 4.lqrmin 5.rrpwr

0.006 0.006 30.00 -30.00 10.00

@! / 6.Te 7.lmax

0.006 1.00/

@! /-----

933631 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

@! / ----- ICONS -----

@! / 1.PFflag 2.Vflag 3.Qflag 4.Pflag 5.PQflag 6.VcmpFlag
 0 0 0 0 0 0

@! / ----- CONS -----

@! / 1.Vdip 2.Vup 3.Trv 4.dbd1 5.dbd2
 0.8500 1.4000 0.0060 -0.001 0.001

@! / 6.Kqv 7.lqh1 8.lql1 9.Vref0 10.lqfrz
 2.0000 2.0000 -2.0000 0.0000 0.0000

@! / 11.Thld 12.Thld2 13.Tp 14.QMax 15.QMin
 0.0000 0.0000 0.0060 1.0000 -1.0000

@! / 16.Vmax 17.Vmin 18.Kqp 19.Kqi 20.Kvp
 1.2000 -1.2000 1.0000 5.0000 1.0000

@! / 21.Kvi 22.Vbias 23.Tiq 24.dPmax 25.dPmin
 5.0000 0.0000 0.0060 30.000 -30.000

@! / 26.Pmax 27.Pmin 28.lmax 29.Tpord 30.Vq1
 1.0000 -1.0000 1.2000 0.0250 0.1000

@! / 31.lq1 32.Vq2 33.lq2 34.Vq3 35.lq3
 1.0000 1.1000 1.0000 0.0000 0.0000

@! / 36.Vq4 37.lq4 38.Vq5 39.lq5 40.Vq6
 0.0000 0.0000 0.0000 0.0000 0.0000

@! / 41.lq6 42.Vq7 43.lq7 44.Vq8 45.lq8
 0.0000 0.0000 0.0000 0.0000 0.0000

@! / 46.Vq9 47.lq9 48.Vq10 49.lq10 50.Vp1
 0.0000 0.0000 0.0000 0.0000 0.1000

@! / 51.lp1 52.Vp2 53.lp2 54.Vp3 55.lp3
 1.0000 1.1000 1.0000 0.0000 0.0000

@! / 56.Vp4 57.lp4 58.Vp5 59.lp5 60.Vp6
 0.0000 0.0000 0.0000 0.0000 0.0000

@! / 61.lp6 62.Vp7 63.lp7 64.Vp8 65.lp8
 0.0000 0.0000 0.0000 0.0000 0.0000

@! / 66.Vp9 67.lp9 68.Vp10 69.lp10 70.Rc
 0.0000 0.0000 0.0000 0.0000 0.0000

@! / 71.Xc 72.Tr1 73.Kc 74.Ke 75.Vblk
 0.0000 0.0060 0.0000 1.0000 0.5000

@! / 76.Vblkh 77.Tblk
 1.1000 0.0000/

993363101 'VTGTPAT' 933631 933631 D3 -1 1.2 0.16 0.0 /
 993363102 'VTGTPAT' 933631 933631 D3 -1 1.1 2 0.0 /
 993363103 'VTGTPAT' 933631 933631 D3 0.5 5 1.1 0.0 /
 993363104 'VTGTPAT' 933631 933631 D3 0.88 5 3 0.0 /
 993363105 'FRQTPAT' 933631 933631 D3 56.5 100 0.16 0.0 /
 993363106 'FRQTPAT' 933631 933631 D3 58.5 100 300 0.0 /

993363107 'FRQTPAT' 933631 933631 D3 -100 61.2 300 0.0 /
993363108 'FRQTPAT' 933631 933631 D3 -100 62 0.16 0.0 /

///NEP-22-G03-033

933681 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/933681 'REPCA1' D3

/1111 101 1111 '1' 1 0 1

/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0

/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933681 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

0 1 0 0 1 0

0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0

0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9

0 0.02 99 -99 1 -1 1.2 0.02

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993368101 'VTGTPAT' 933681 933681 D3 -1 1.2 0.16 0.0 /

993368102 'VTGTPAT' 933681 933681 D3 -1 1.1 2 0.0 /

993368103 'VTGTPAT' 933681 933681 D3 0.5 5 1.1 0.0 /

993368104 'VTGTPAT' 933681 933681 D3 0.88 5 3 0.0 /

993368105 'FRQTPAT' 933681 933681 D3 56.5 100 0.16 0.0 /

993368106 'FRQTPAT' 933681 933681 D3 58.5 100 300 0.0 /

993368107 'FRQTPAT' 933681 933681 D3 -100 61.2 300 0.0 /

993368108 'FRQTPAT' 933681 933681 D3 -100 62 0.16 0.0 /

///NEP-22-G03-020

933901 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1

0.02 0.02 99 -99 10.0 0.01 1.0/

/933901 'REPCA1' D3

/1111 101 1111 '1' 1 0 1

/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0

/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

933901 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

0 1 0 0 1 0

0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0

0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9

0 0.02 99 -99 1 -1 1.2 0.02

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993390101 'VTGTPAT' 933901 933901 D3 -1 1.2 0.16 0.0 /

993390102 'VTGTPAT' 933901 933901 D3 -1 1.1 2 0.0 /

993390103 'VTGTPAT' 933901 933901 D3 0.5 5 1.1 0.0 /

993390104 'VTGTPAT' 933901 933901 D3 0.88 5 3 0.0 /

993390105 'FRQTPAT' 933901 933901 D3 56.5 100 0.16 0.0 /

993390106 'FRQTPAT' 933901 933901 D3 58.5 100 300 0.0 /

993390107 'FRQTPAT' 933901 933901 D3 -100 61.2 300 0.0 /

993390108 'FRQTPAT' 933901 933901 D3 -100 62 0.16 0.0 /

///NEP-22-G03-021

993901 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1

0.02 0.02 99 -99 10.0 0.01 1.0/

/993901 'REPCA1' D3

/1111 101 1111 '1' 1 0 1

/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0

/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

993901 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20

0 1 0 0 1 0

0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0

0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9

0 0.02 99 -99 1 -1 1.2 0.02

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01

0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

999390101 'VTGTPAT' 993901 993901 D3 -1 1.2 0.16 0.0 /
999390102 'VTGTPAT' 993901 993901 D3 -1 1.1 2 0.0 /
999390103 'VTGTPAT' 993901 993901 D3 0.5 5 1.1 0.0 /
999390104 'VTGTPAT' 993901 993901 D3 0.88 5 3 0.0 /
999390105 'FRQTPAT' 993901 993901 D3 56.5 100 0.16 0.0 /
999390106 'FRQTPAT' 993901 993901 D3 58.5 100 300 0.0 /
999390107 'FRQTPAT' 993901 993901 D3 -100 61.2 300 0.0 /
999390108 'FRQTPAT' 993901 993901 D3 -100 62 0.16 0.0 /

///NEP-22-G03-044
930851 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/930851 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

930851 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

993085101 'VTGTPAT' 930851 930851 D3 -1 1.2 0.16 0.0 /
993085102 'VTGTPAT' 930851 930851 D3 -1 1.1 2 0.0 /
993085103 'VTGTPAT' 930851 930851 D3 0.5 5 1.1 0.0 /
993085104 'VTGTPAT' 930851 930851 D3 0.88 5 3 0.0 /
993085105 'FRQTPAT' 930851 930851 D3 56.5 100 0.16 0.0 /
993085106 'FRQTPAT' 930851 930851 D3 58.5 100 300 0.0 /
993085107 'FRQTPAT' 930851 930851 D3 -100 61.2 300 0.0 /
993085108 'FRQTPAT' 930851 930851 D3 -100 62 0.16 0.0 /

///NEP-22-G03-043
990851 'USRMDL' D3 'REGCBU1' 101 1 2 7 5 8 0 1
0.02 0.02 99 -99 10.0 0.01 1.0/

/990851 'REPCA1' D3
/1111 101 1111 '1' 1 0 1
/0.02 0 0 0 0.02 0 0 0 0 999 -999 0 0
/0 0 0.5 0.25 0.02 -0.0006 0.0006 999 -999 1 -1 0.02 20 20/

990851 'USRMDL' D3 'REECDU1' 102 0 6 77 7 20
0 1 0 0 1 0
0.4 1.3 0.02 -0.10 0.10 1 1.0 -1.0 0.00 0
0 0 0.01 0 0 1.05 0.95 0.9 0.9 0.9 0.9
0 0.02 99 -99 1 -1 1.2 0.02
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.499 0.01 0.5 1 0.6 1 0.9 1 1 1 1.1 1 1.2 1 1.201 0.01 1.3 0.01
0.01 0.01 0.02 0.01 1 0.5 1.1 0.04/

999085101 'VTGTPAT' 990851 990851 D3 -1 1.2 0.16 0.0 /
999085102 'VTGTPAT' 990851 990851 D3 -1 1.1 2 0.0 /
999085103 'VTGTPAT' 990851 990851 D3 0.5 5 1.1 0.0 /
999085104 'VTGTPAT' 990851 990851 D3 0.88 5 3 0.0 /
999085105 'FRQTPAT' 990851 990851 D3 56.5 100 0.16 0.0 /
999085106 'FRQTPAT' 990851 990851 D3 58.5 100 300 0.0 /
999085107 'FRQTPAT' 990851 990851 D3 -100 61.2 300 0.0 /
999085108 'FRQTPAT' 990851 990851 D3 -100 62 0.16 0.0 /

This appendix has been redacted for Critical Energy/
Electric Infrastructure Information (CEII).

Appendix D – N-0 and N-1 Thermal and Voltage Results

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Appendix E – Stability Analysis Plots

WMA Group 3 cluster stability plots_pdf.zip

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Electric Infrastructure Information (CEII).

Appendix F – PSCAD Analysis Report

Western MA DER Group 3 PSCAD Report 5_20_2022.pdf